

Mathematical models of the human lungs

B. Maury

Laboratoire de Mathématiques, Université Paris-Sud

C. Grandmont, S. Martin, D. Salort, C. Vannier

T. Similowski, C. Strauss

ACINIM LePoumonVousDisJe

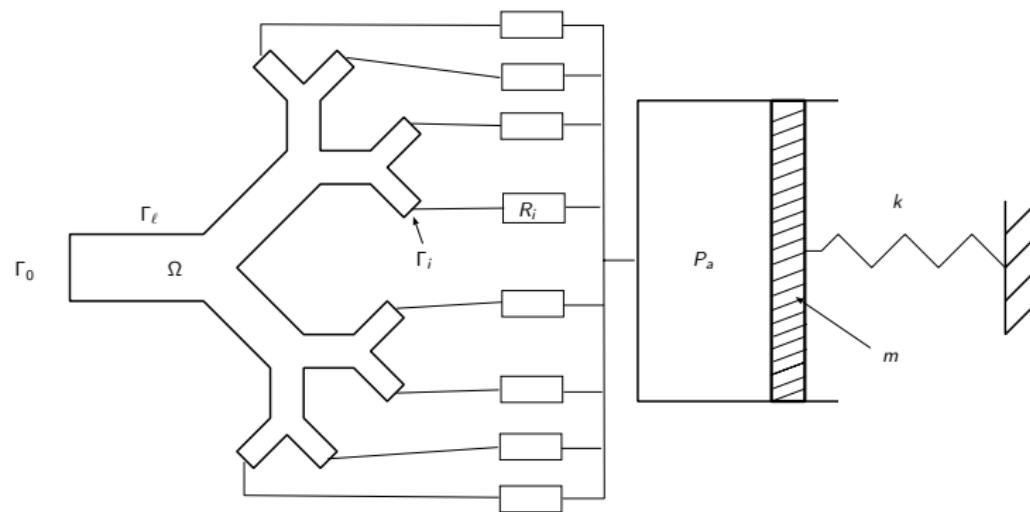
Optimal Transport in the Human Body: Lungs and Blood

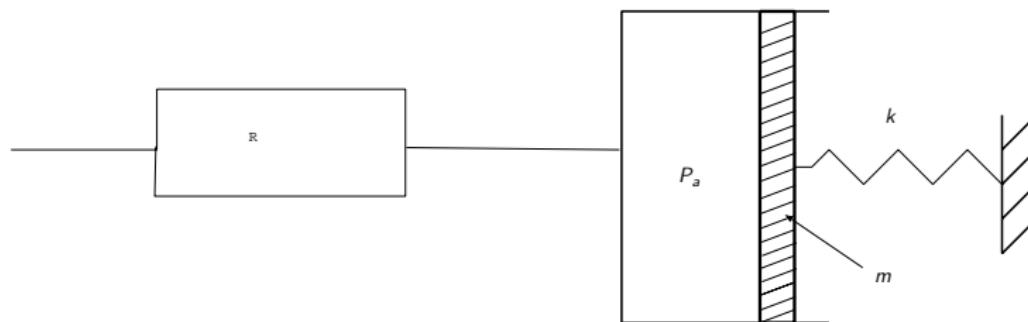
May 19 - 23, 2008

1 0D model

2 Infinite tree model

3 Fully coupled model





Poiseuille's law : $0 - P_a = R \times \text{flux} = RS\dot{x}$.

Force exerted on the piston : SP_a .

OD MODEL (WITH T. SIMILOVSKI, C. STRAUSS)

$$m\ddot{x} + (RS^2 + \mu)\dot{x} + kx = f(t).$$

A. Ben-Tal, *J. Theor. Biol.* 2006

J.R. Rodarte, K. Rehder, *Handbook of physiology*, 1986.

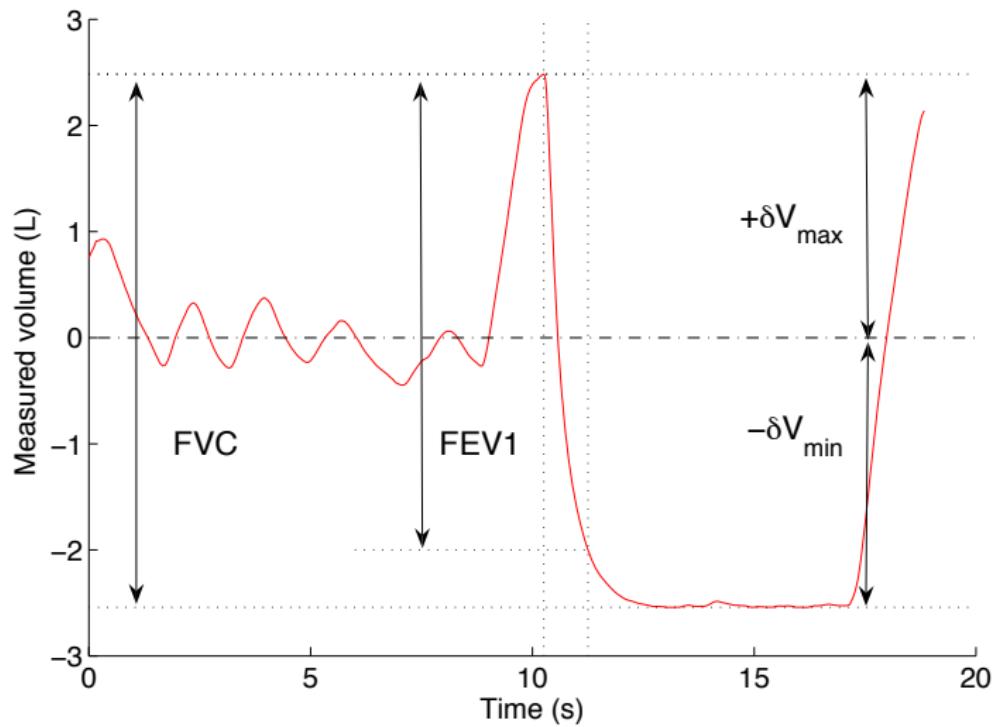
J.B. West, *Resp. Physiol. - The Essentials'*, 1974.

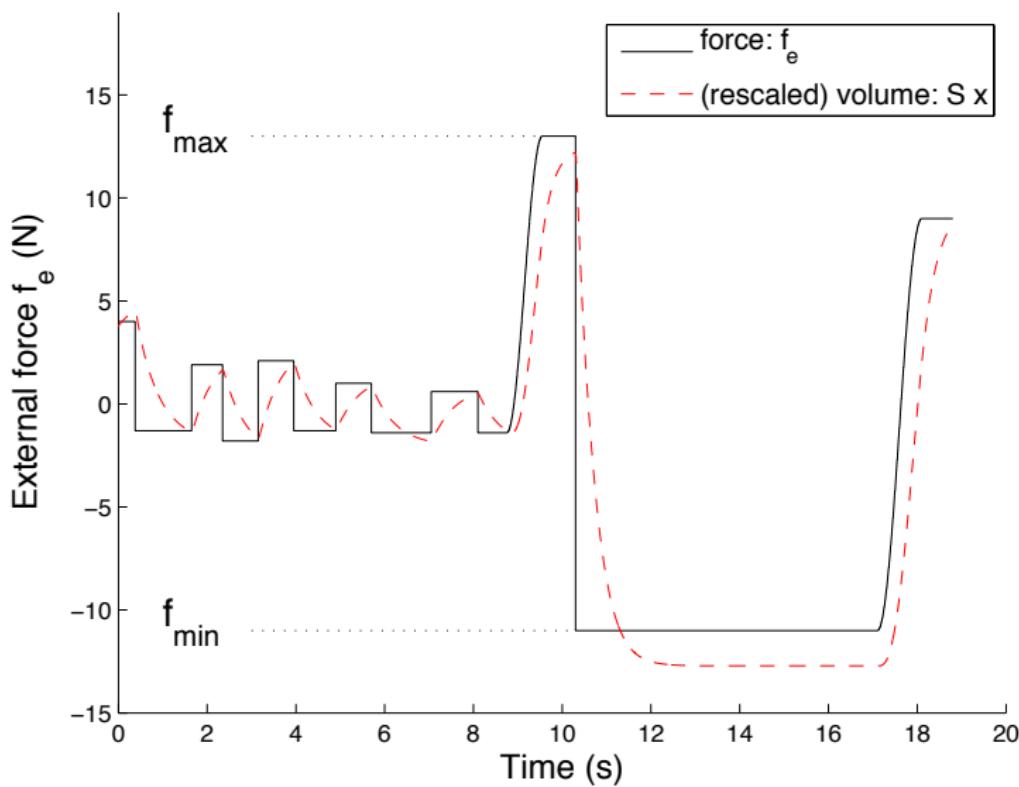
E.R. Weibel, *Morphometry of the human lung*, 1963.

$$m = 0.3 \text{ kg}, \quad S = 0.011 \text{ m}^2, \quad k_0 = 36.3 \text{ N} \cdot \text{m}^{-1},$$

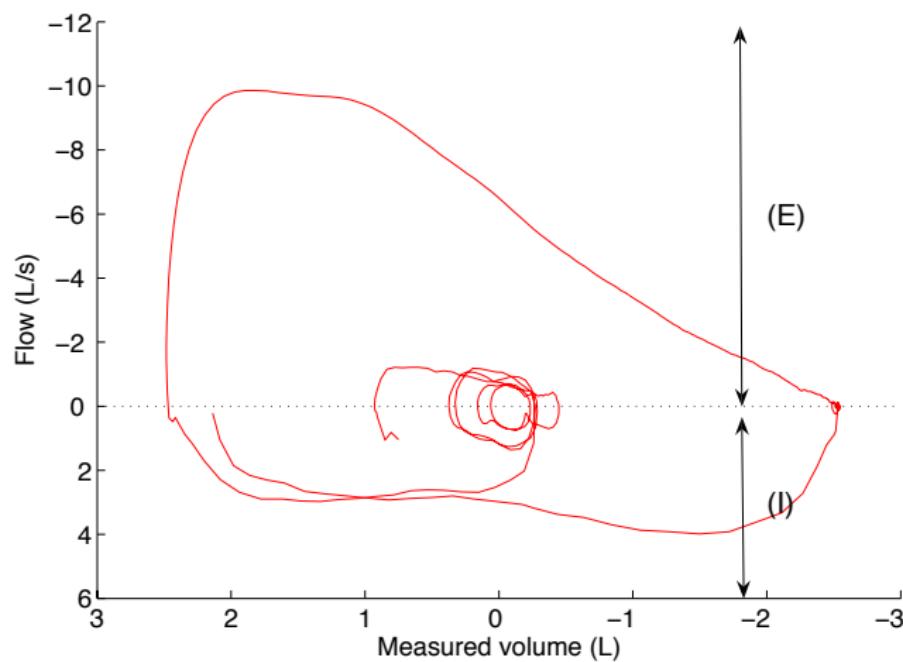
$$R = 1.33 \cdot 10^5 \text{ Pa} \cdot \text{s} \cdot \text{m}^{-3}, \quad \mu = 4.02 \text{ Pa} \cdot \text{s} \cdot \text{m}.$$

N.B. Nonlinear stiffness $k(x)$ used in practice

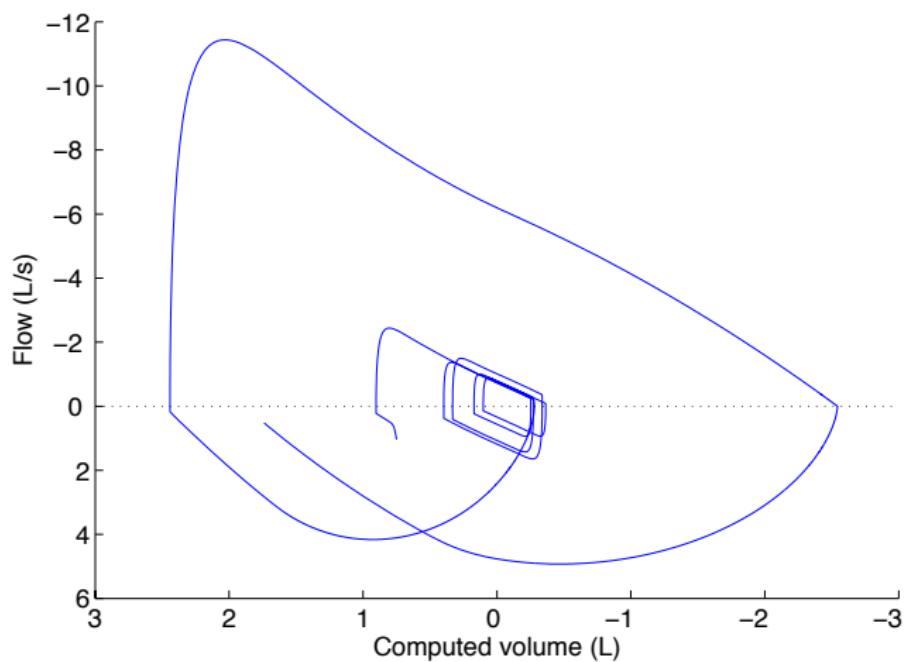




FLOW VOLUME LOOP (EXP.)



FLOW VOLUME LOOP (NUM.)



EXTENSIONS

Two compartment model : T. Similowski, J.H.T. Bates,

Two-compartment modelling of respiratory system mechanics at low frequencies : gas redistribution or tissue rheology ?, Eur. Respir. J. (1991)

Gas transport / diffusion : A. Ben-Tal, *Simplified models for gas exchange in the human lungs, J. Theor. Biol. (2006)*

Smooth muscle (B.M, S.M, T. Similowski, C. Strauss)

Oxygen impoverishment

NON-CONSTANT RESISTANCE

Total volume variation $\delta V = Sx$: sum of δV_A (for the alveoli) and δV_B (for the bronchi) with

$$\delta V_A = (1 - \theta) Sx, \quad \delta V_B = \theta Sx.$$

θ close to 0 : the branches are rigid.

Resistance of a pipe proportional to L/D^4 :

It varies like the reciprocal of the volume (for a given shape), one has

$$R(x) = \frac{R_0}{1 + \theta Sx/V_B^0}.$$

For compliant branches (neutral value $\theta_0 = V_A^0/(V_A^0 + V_B^0)$), the resistance decreases significantly during inspiration.

Smooth muscle limits this decrease : apparently counter-productive.

For lower values of θ (action of the smooth muscle), the resistance is higher, but the exchange area is also likely to be larger
→ improved gaz exchange.

Assumption : the quantity of diffused O_2 is proportional to the total alveolar wall area, which scales like $V_A^{2/3}$:

$$q = \int_0^t \left(1 + (1 - \theta)Sx/V_B^0\right)^{2/3} dt.$$

GLOBAL SYSTEM

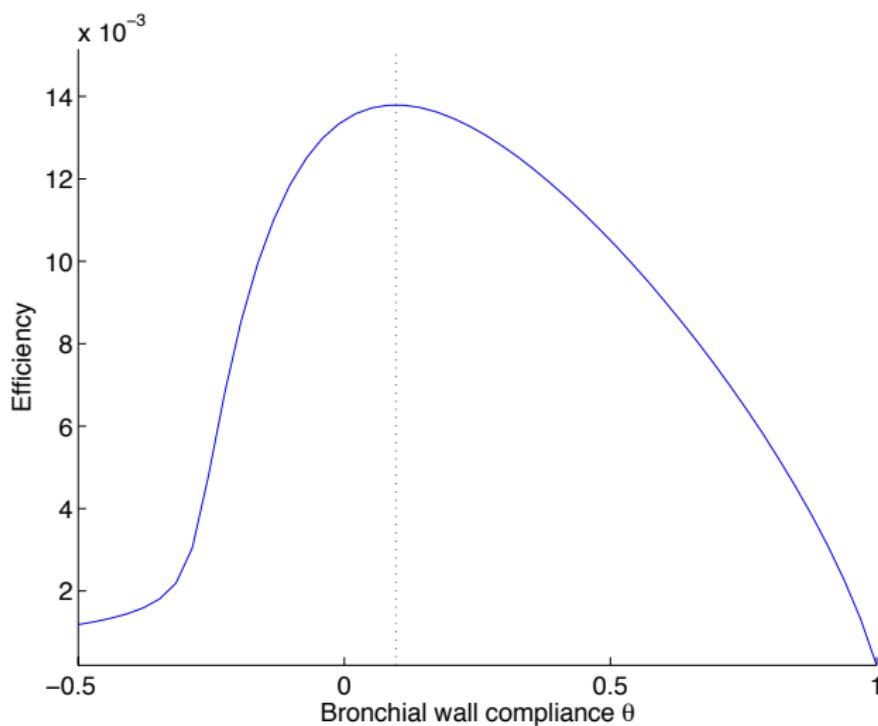
$$\begin{cases} m\ddot{x} + \left(\frac{R_0 S^2}{1 + \theta Sx/V_B^0} + \mu \right) \dot{x} + kx = f_e \\ \dot{q} = (V_A^0 + (1 - \theta)Sx)^{2/3} \end{cases}$$

Efficiency : $q = \int_0^T \dot{q} dt$.

θ large \rightarrow compliant branches \rightarrow small resistance but also small exchange area.

θ small \rightarrow rigid branches \rightarrow large resistance but also larger exchange area.

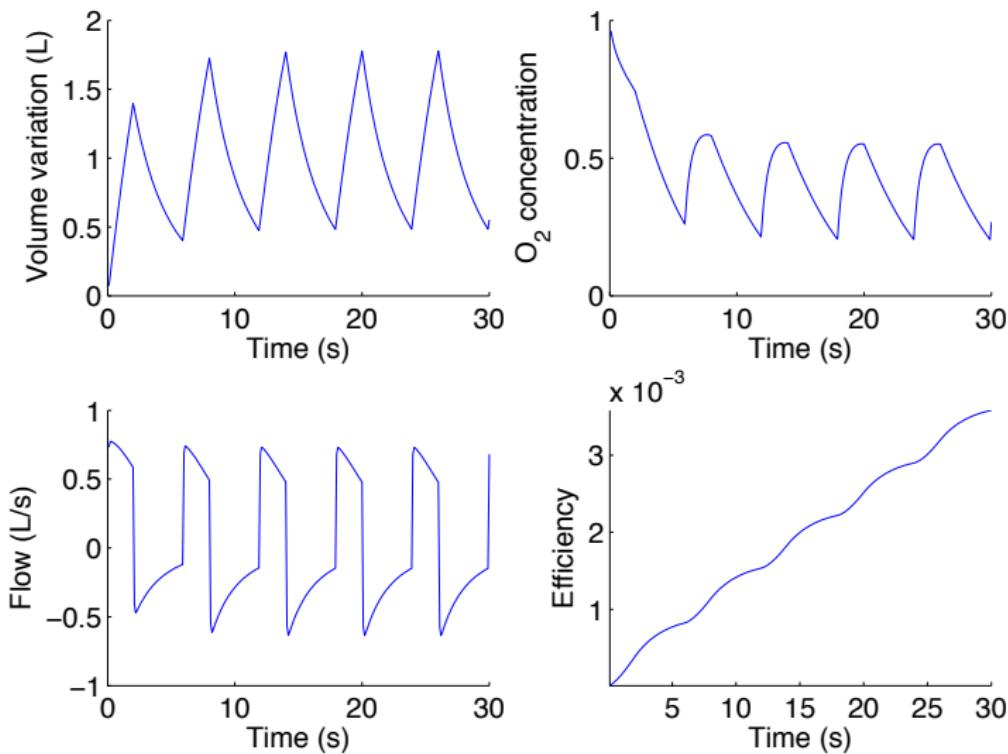
Neutral value ≈ 0.4 .



O_2 IMPOVERTISHMENT

Concentration c of O_2 in the alveoli is not constant :
 impoverishment by diffusion through alveolar membrane
 + tidal exchange : fresh air at c_0 during inspiration
 impoverished air at c during expiration

$$\begin{cases} \dot{x} = u \\ \dot{u} = \frac{1}{m} \left(f_e - \left(\frac{R_0 S^2}{1 + \theta Sx/V_B^0} + \mu \right) u - kx \right) \\ \dot{q} = \Lambda (V_A^0 + (1 - \theta)Sx)^{2/3} c \\ \dot{c} = \frac{1}{V_A} (\dot{V}_A (c_0 - c) \mathbf{1}_{\mathbb{R}^+}(u) - \dot{q}) . \end{cases}$$



Questions : $T > 0$ is fixed, consider f_e as a control

Maximize $q(T)$ with respect to f_e , under the constraint
 $W = \int_0^T \dot{x} f_e = W_0$ fixed.

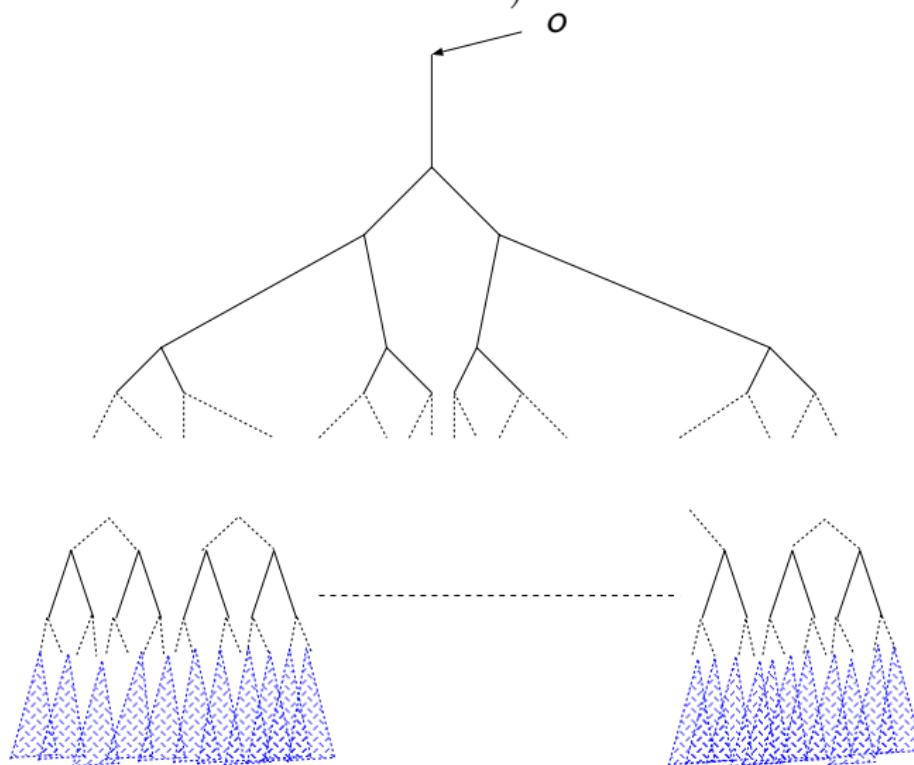
Maximize $q(T)$ with respect to f_e , under the constraint
 $|f_e| \leq F_{max}$.

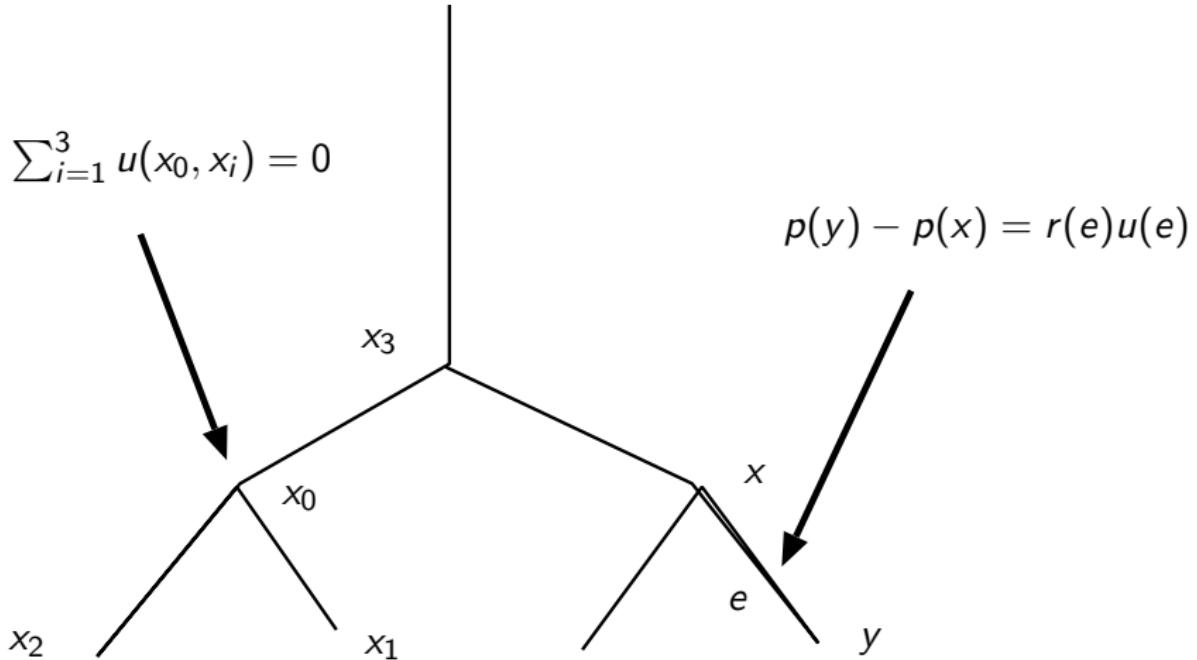
Is f_e (quasi-)periodic ?

Does forced expiration occur ?

How does it evolve as R is increasing ?

INFINITE RESISTIVE INFINITE TREE (WITH D. SALORT & C. VANNIER)





V set of vertices, $E \subset V \times V$ set of edges.

Resistance field $R = (r(e))_{e \in E}$, symmetric, $r(e) \in (0, +\infty)$.

Pressure $p : V \longrightarrow \mathbb{R}$

Flux $u \in \mathbb{R}^E$, $(u(y, x) = -u(x, y))$,

Divergence and gradient operators :

$$\partial : \mathbb{R}^E \longrightarrow \mathbb{R}^V$$

$$u \longmapsto \partial u, \quad \partial u(x) = \sum_{y \sim x} u(x, y)$$

$$\partial^* : \mathbb{R}^V \longrightarrow \mathbb{R}^E$$

$$p \longmapsto \partial^* p, \quad \partial^* p(e) = \partial^* p(x, y) = p(y) - p(x)$$

Poiseuille's Law : $u = -r^{-1}\partial^* p$

Kirchhoff's law : $\partial u = 0$

Ventilation model :

$$\begin{cases} u + c \partial^* p &= 0 \\ \partial u &= \delta_0. \end{cases}$$

Functional spaces :

$$L^2(T) = \left\{ u \in \mathbb{R}^E, \sum_e r(e) |u(e)|^2 < +\infty \right\},$$

$$H^1(T) = \left\{ p \in \mathbb{R}^V, |p|_1^2 = \sum_e c(e) |p(y) - p(x)|^2 < +\infty \right\}$$

L^2 : weighted ℓ^2 space

H^1 Hilbert space for $\|p\|^2 = p(0)^2 + |p|_1^2$

Poiseuille's Law : $u = -r^{-1}\partial^* p$

$$\mathbf{u} = -k\nabla p$$

Kirchhoff's law : $\partial u = 0$

$$\nabla \cdot \mathbf{u} = 0$$

Ventilation model :

$$\left\{ \begin{array}{lcl} u + c \partial^* p & = & 0 \\ \partial u & = & \delta_0 \end{array} \right. \longleftrightarrow \left\{ \begin{array}{lcl} \mathbf{u} + k \nabla p & = & 0 \\ \nabla \cdot \mathbf{u} & = & \delta_0 \end{array} \right. \quad (\text{Darcy})$$

Functional spaces :

$$L^2(T) = \left\{ u \in \mathbb{R}^E, \sum_e r(e) |u(e)|^2 < +\infty \right\},$$

$$H^1(T) = \left\{ p \in \mathbb{R}^V, |p|_1^2 = \sum_e c(e) |p(y) - p(x)|^2 < +\infty \right\}$$

L^2 : weighted ℓ^2 space

H^1 Hilbert space for $\|p\|^2 = p(0)^2 + |p|_1^2$

T : infinite dyadic tree

H_0^1 : closure of $D(T)$ (finitely supported fields) in H^1 .

Question : is H_0^1 different from H^1 ?

Or : is $\tilde{H}^{1/2} = H^1/H_0^1$ different from $\{0\}$?

Yes \iff the effective resistance is finite

For a regular geometric tree ($r_N = r_0 \alpha^N = r_0/h^{3N}$) :

yes iff $h > 1/\sqrt[3]{2} \approx 0.79$.

N.B. $\sqrt[3]{2}$ is the critical value in

Mauroy, Filoche, Weibel, Sapoval, Nature '2004

The condition holds true for $h = 0.85$.

Under the assumption that the effective resistance is finite

$$\begin{cases} u + c \partial^* p = 0 \\ \partial u = \delta_0 \\ \tilde{\gamma}_0 p = \tilde{g} \quad \text{on } \Gamma \end{cases}$$

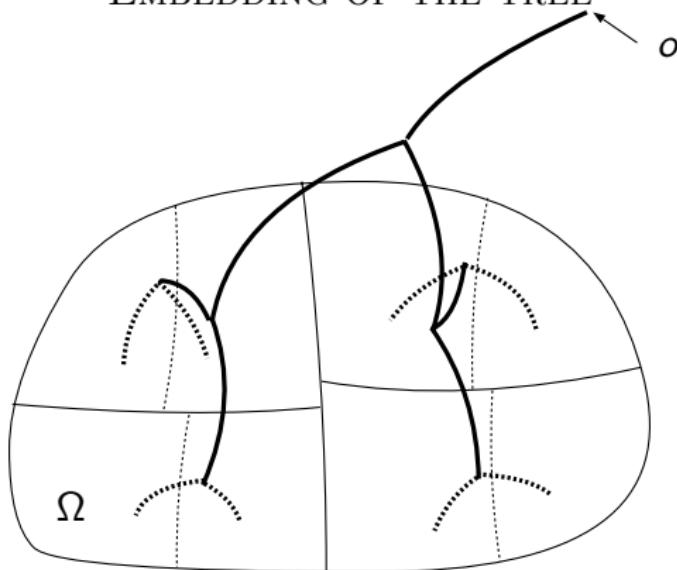
is well-posed, but purely abstract

How to describe $H^{1/2}$, space of pressures defined on the set of leafs

Semi abstract approach :

$H^{1/2}$ can be identified to a subset of $L^2(\Gamma)$, where Γ is the set of ends (set of paths to infinity = $\{0, 1\}^{\mathbb{N}}$).

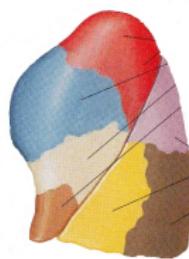
EMBEDDING OF THE TREE



REGULARITY OF THE “REAL” PRESSURE FIELD

Main idea : $\Gamma = \{0, 1\}^{\mathbb{N}}$ is imbedded in a given domain Ω

Human lung



Modelling :

$$\Omega \subset \mathbb{R}^d$$

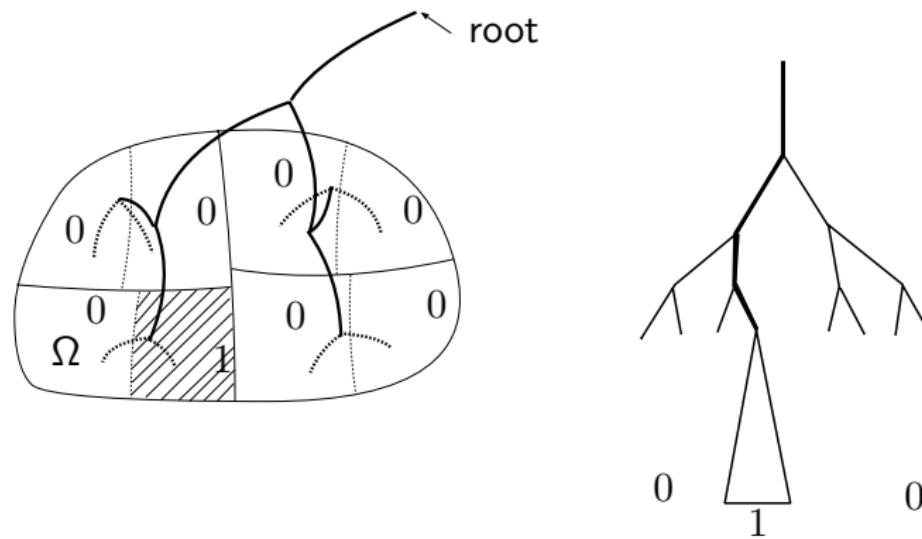
$N \geq 1$ index of the generation

A partition $(\Omega_N^j)_{j \in \{0 \dots 2^N - 1\}}$ of Ω is given with the following hierarchical structure :

$$\Omega_{N+1}^{2k} \cup \Omega_{N+1}^{2k+1} = \Omega_N^k$$

IMBEDDING OF THE TREE

One considers the set F of functions which are piecewise constant at infinity : spanned by



It defines a mapping

$$\gamma : F \subset H^1(T) \longrightarrow L^2(\Omega).$$

Prop.

If the tree is regular, and if the decomposition is balanced :

$$|\Omega_j^n| = 2^{-n}$$

γ can be extended by density to a continuous mapping

$$\gamma : H^1(T) \longrightarrow L^2(\Omega).$$

REGULARITY OF THE CONTINUOUS PRESSURE FIELD

By using Besov-type characterization of H^s :

Prop.

Regular tree, geometric increase of pipe resistances

$\gamma(H^1) = H^s(\Omega)$ with

$$s = d \left(\frac{1}{2} - \frac{\ln(\alpha)}{2\ln 2} \right).$$

Regularity for the human lung :

reduction coefficient : $h \simeq 0.85$

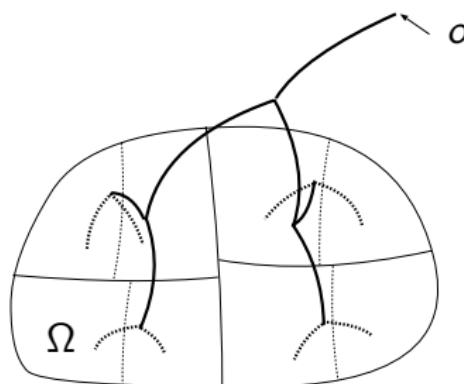
geometric resistances : $\alpha = \frac{1}{h^3} \simeq 1.63$

It yields $s \simeq 0.45$: pressure field in $H^s(\Omega)$.

It leads to the following “elliptic” problem

$g \in H^{0.45}(\Omega)$ prescribed pressure field within the parenchyma Ω

$$\left\{ \begin{array}{l} \text{Find } p \in H^1(T) \text{ s.t. } p(o) = 0, \\ -\partial c \partial^* p = 0 \quad \text{in} \quad T \setminus \{o\}, \\ \gamma(p) = g. \end{array} \right.$$



Fluxes : $\Phi(\Omega_N^k)$ obtained from p , for any subdomain Ω_N^k .

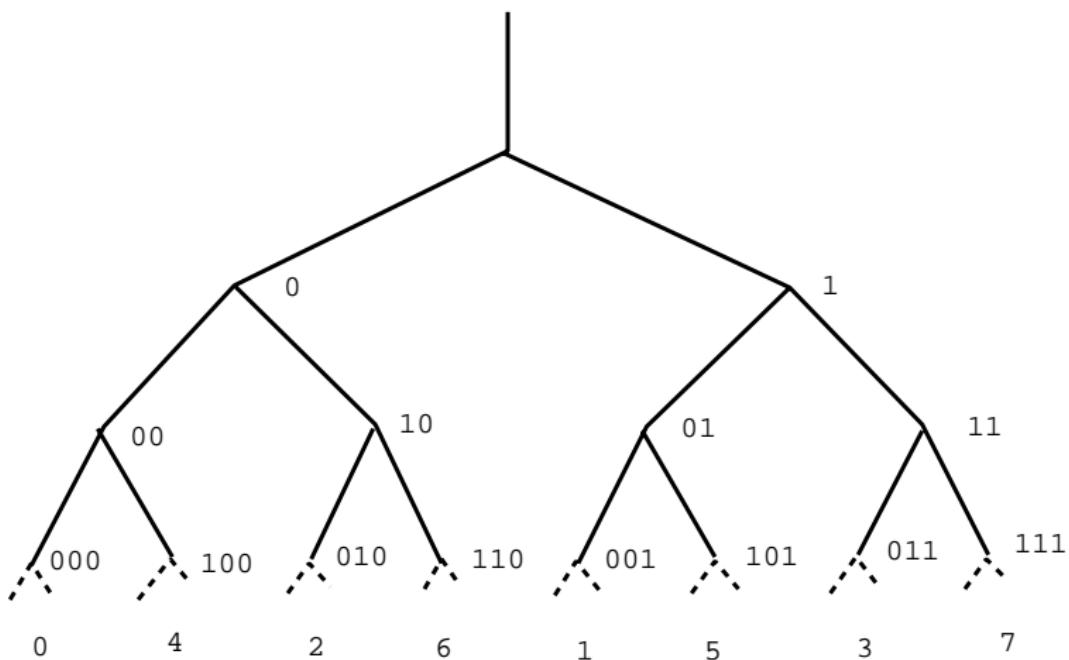
ALGEBRAIC FRAMEWORK

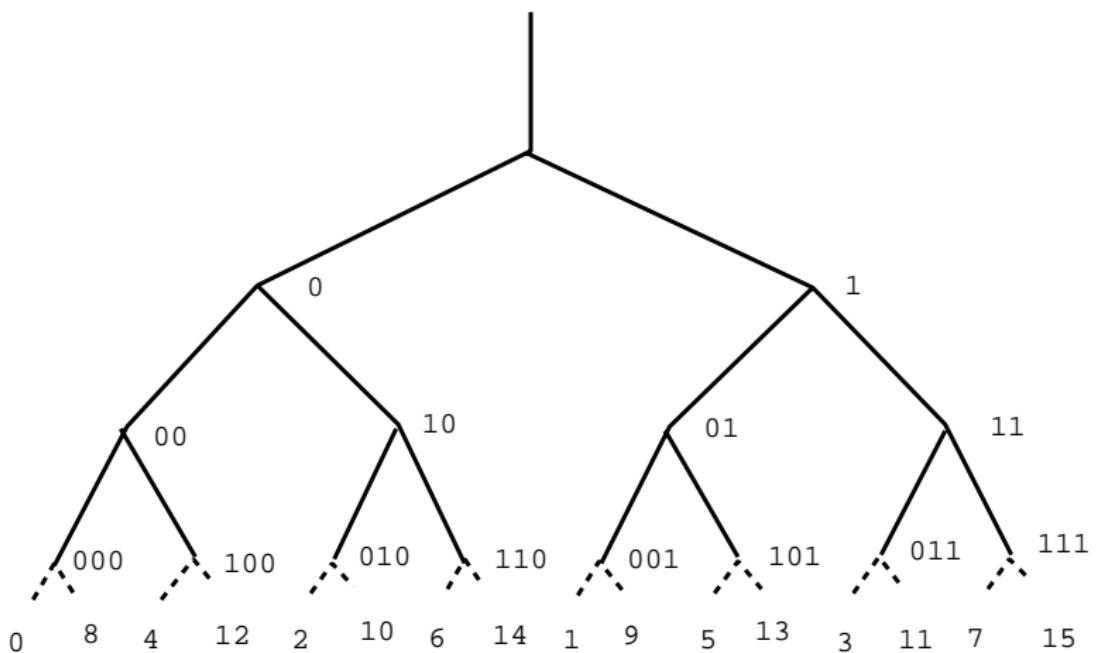
Goal : set up a framework which accounts for the notion of proximity (between leafs) with respect to the tree.

By-product : explicit formula for the mapping

fluxes at the ends \longmapsto pressure field

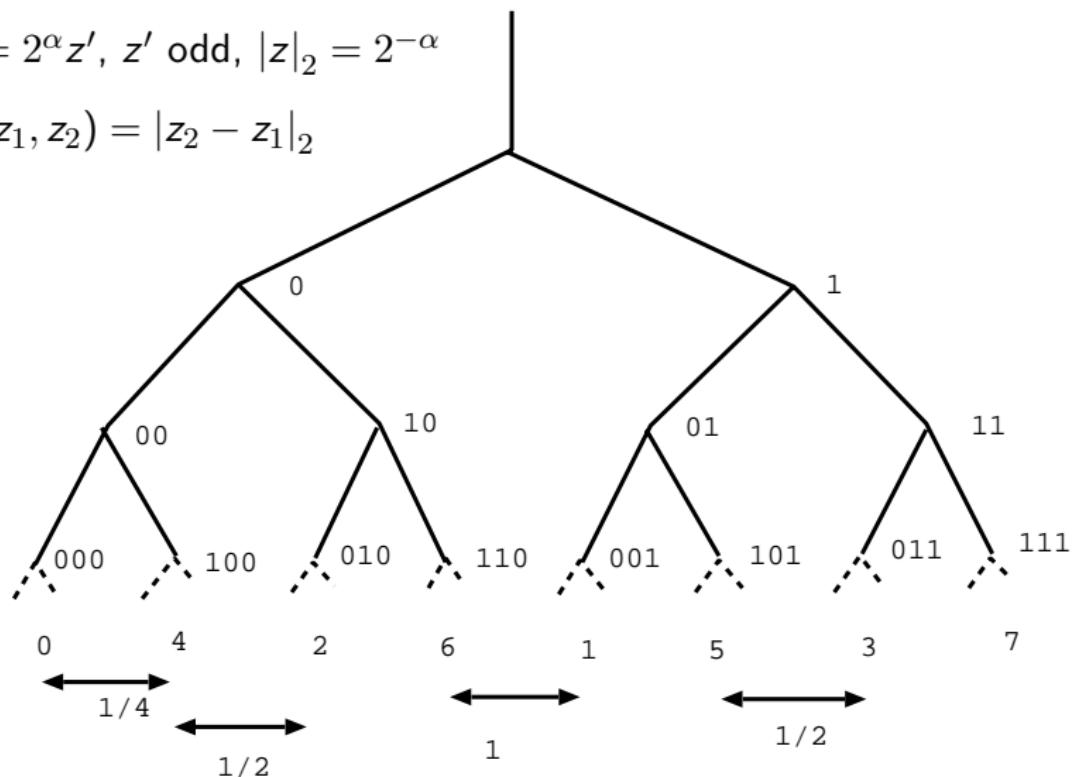
Extension of a previous work (with C. Grandmont and N. Meunier)





If $z = 2^\alpha z'$, z' odd, $|z|_2 = 2^{-\alpha}$

$$\text{dist}(z_1, z_2) = |z_2 - z_1|_2$$



$$\Gamma_N = \{0, 1, \dots, 2^N - 1\} \subset \mathbb{Z}$$

equipped with ultra metric-distance

$$z = 2^\alpha y, \quad 2 \nmid y, \quad |z|_2 = 2^{-\alpha}, \quad \text{dist}(z_1, z_2) = |z_2 - z_1|_2.$$

One has

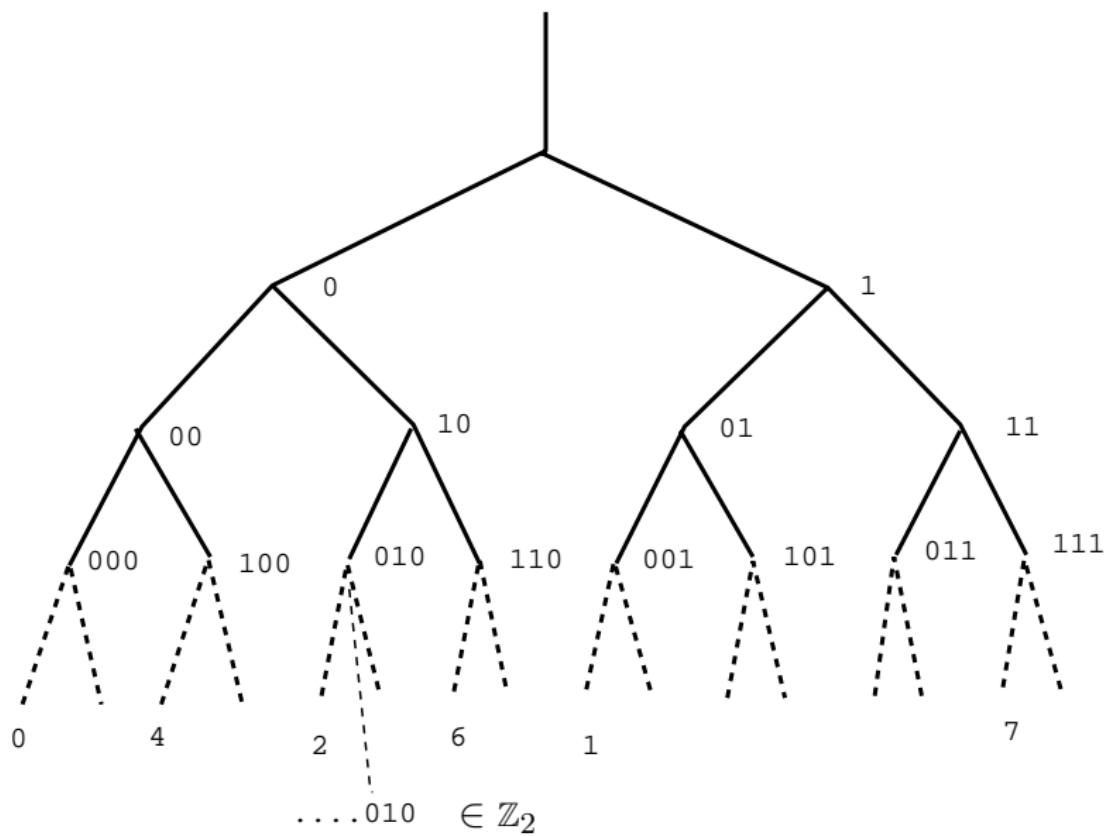
$$\overline{\bigcup_{N \in \mathbb{N}} \Gamma_N} = \mathbb{Z}_2 \quad \text{set of dyadic integers}$$

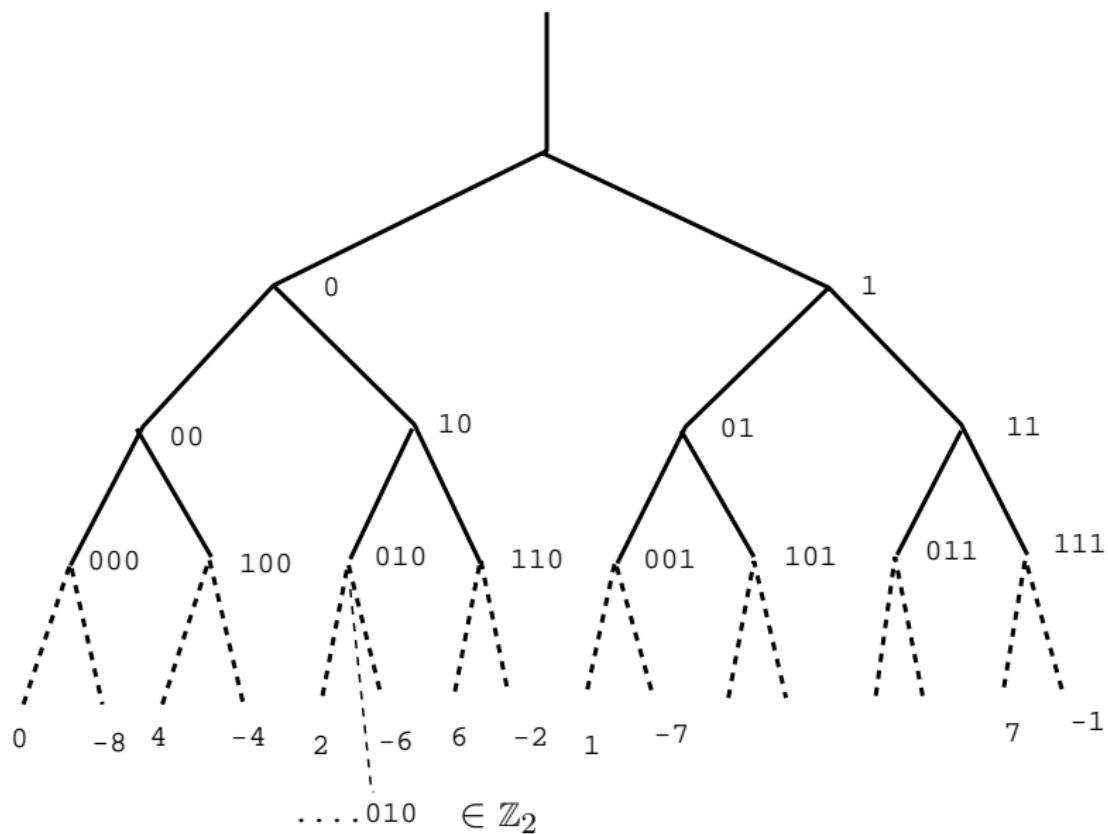
More properly :

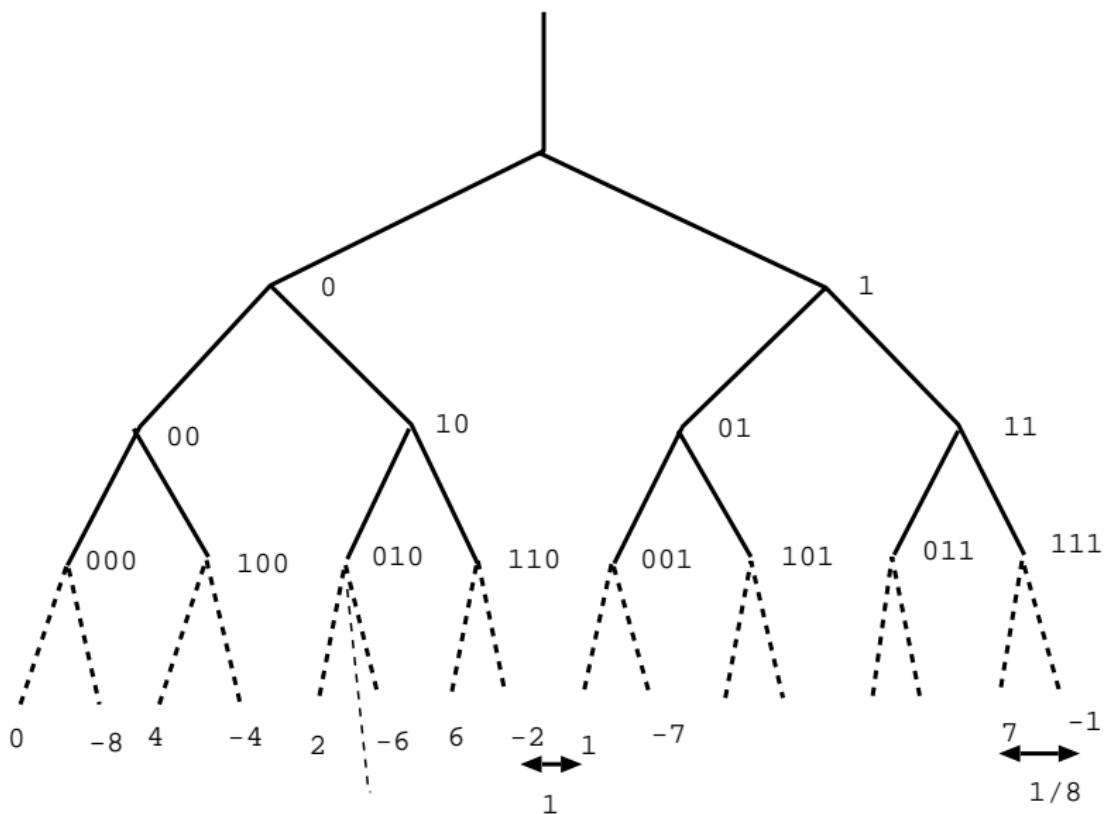
$$\Gamma_n = \mathbb{Z}/2^n \mathbb{Z}, \quad \varphi_{nm} : z \in \Gamma_m \longmapsto \tilde{z} \in \Gamma_n \quad (\tilde{z} \equiv z \pmod{2^n}) \quad n \leq m.$$

Γ is the projective limit of the Γ_n 's :

$$\Gamma = \varprojlim \Gamma_n = \left\{ (a_n) \in \prod_{n \in \mathbb{N}} \Gamma_n, \quad \varphi_{nm}(a_m) = a_n \quad \forall n \leq m \right\}$$







Notion of integral over \mathbb{Z}_2 , based on

$$\int_{\mathbb{Z}_2} \mathbb{1}_{a+2^n\mathbb{Z}_2} = 2^{-n}$$

Fluxes : $\mu \in \mathcal{M}(\mathbb{Z}_2) : \mu(a + 2^n\mathbb{Z}_2)$ is known

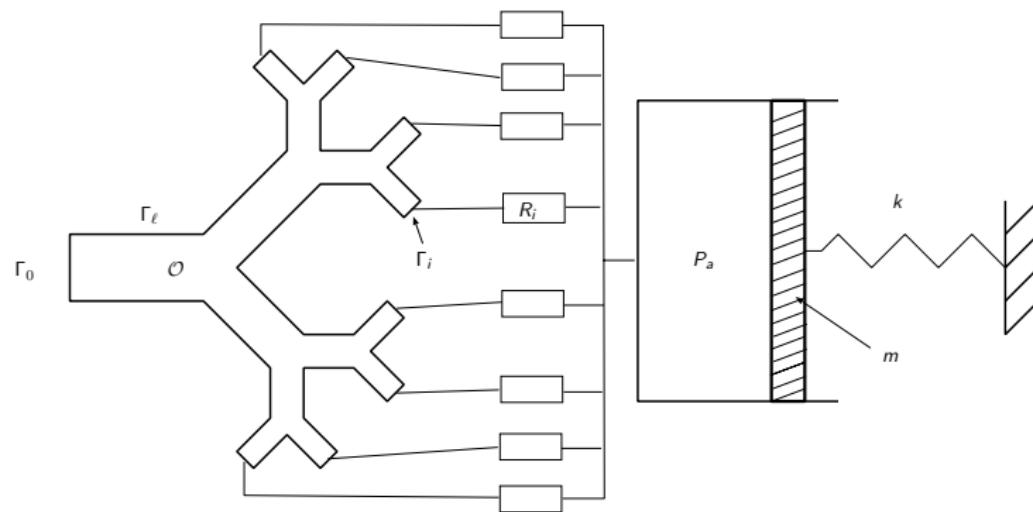
$$p(x) = \mathcal{R}\mu(x) = \int_{\mathbb{Z}_2} \frac{\mu(y)}{|x - y|^{\log_2(\alpha)}} dy = G \star \mu(x).$$

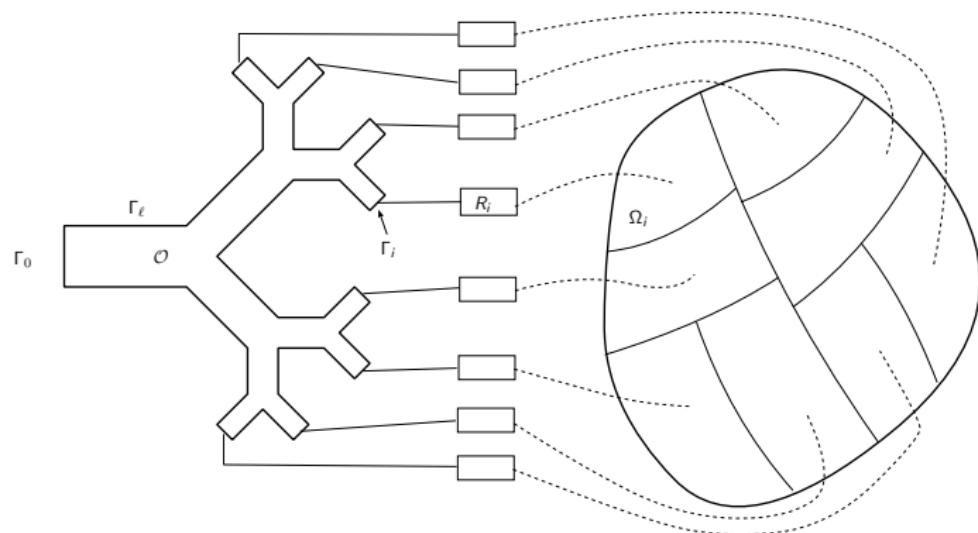
where G is a Green-like Kernel (like $1/|x - y|^{d-2}$ in \mathbb{R}^d).

N.B. : for $R < \infty$, $\log_2(\alpha) \in (-\infty, 1)$

In particular $\log_2(\alpha) \approx 0.7$ for $\alpha = 0.85$

“Equivalent” dimension $d = 2.7$





\mathbf{d} : displacement field in the parenchyma

$P = \sum P_i \mathbb{1}_{\Omega_i}$ outlet pressures (on Γ_i)

$\Pi = \sum \Pi_i \mathbb{1}_{\Omega_i}$ pressure field in the parenchyma

$$P_i - \Pi_i = \mathcal{R}_i \nabla \cdot \partial_t \mathbf{d}$$

$$\begin{aligned} \rho \partial_{tt} \mathbf{d} - k \nabla \cdot (\nabla \mathbf{d} + \nabla^T \mathbf{d}) + \nabla \Pi &= 0 \quad \text{in } \Omega \\ \mathbf{d} &\text{ prescribed on } \partial \Omega. \end{aligned}$$

$$\begin{aligned} \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} - \mu \Delta \mathbf{u} + \nabla p &= 0 \text{ in } \mathcal{O} \\ \nabla \cdot \mathbf{u} &= 0 \text{ in } \mathcal{O}. \end{aligned}$$

$$\begin{cases} \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} = 0 & \text{on } \Gamma_0 \\ \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} = -P_i \mathbf{n} & \text{on } \Gamma_i \end{cases}$$

$$\int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} = \int_{\Omega_i} \nabla \cdot \partial_t \mathbf{d}$$