Estimation of uncertainties of full moment tensors

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A moment tensor is a 3 x 3 symmetric matrix that characterizes a point-source mechanism for a source such as an earthquake.

Moment tensors can be estimated from ground motion recorded by seismometers. (A model for Earth structure is needed.)

**Why does moment tensor parameterization matter?**

1. Allows for interpretation of the posterior probability density
2. Computational efficiency
3. Accurate numerical integration (dV increment needs to be known)
4. Provides a good framework for visualization
Representation of a recently published new parameterization for moment tensors. Its sampling of model parameter space turns out to be highly non-uniform.
Examples of industry experiments for studying sources

Pesicek et al. (2016)
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Clarke et al. (2013)
\[ \rho \frac{\partial^2 u(x, t)}{\partial t^2} = L_{(x,t)}(u) + f(x, t) \]

seismometer records response \( u = C(f, d) \) at location \( x \)

force couple \( \{f, d\} \) at location \( \xi \)

(\( \xi \) is one of three couples for a moment tensor)

propagation controlled by properties of medium

\[ G(x, t, \xi, \tau, f) \]
A single couple \( \{f, d\} \) is equivalent to two force couples \( \{e_1, M(e_1)\} \) and \( \{e_2, M(e_2)\} \).
Choose any orthonormal basis to get entries of moment tensor matrix.
Notation

\[
[\Lambda] = \begin{pmatrix}
\lambda_1 & 0 & 0 \\
0 & \lambda_2 & 0 \\
0 & 0 & \lambda_3
\end{pmatrix},
\]

\[
[\Lambda]_U = U [\Lambda] U^{-1}.
\]
The symbols $X_\xi$, $Y_\xi$ and $Z_\xi$ denote the rotations through angle $\xi$ about the coordinate axes. Thus

$$Z_\xi = \begin{pmatrix}
\cos \xi & -\sin \xi & 0 \\
\sin \xi & \cos \xi & 0 \\
0 & 0 & 1
\end{pmatrix}, \quad Y_\xi = \begin{pmatrix}
\cos \xi & 0 & \sin \xi \\
0 & 1 & 0 \\
-\sin \xi & 0 & \cos \xi
\end{pmatrix}, \quad \text{etc.}$$

(3)
The moment tensor as slip on a fault
\[ K = R_\phi (e_3) \cdot e_1 = Z_\phi \cdot e_1 \]  
(strike vector)

\[ N = R_\theta (K) \cdot e_3 \]  
(normal vector)

\[ S = R_\sigma (N) \cdot K \]  
(slip vector),

\[ M = \begin{bmatrix} \Lambda \end{bmatrix} Y_{-\pi/4} \]

\[ V(S, N) = (S, N \times S, N), \]
The “orientation block” (3 out of 6 moment tensor parameters)

This will provide all the moment tensor orientations (but half the faults).

Note that the strike, dip, and rake are for the closest double couple of a moment tensor.
Full moment tensors allow for opening (or closing) across a fault.

(Aki and Richards, 1980)

\[ \alpha \] is the angle between slip vector and normal vector:
- \( \alpha = 90 \) for a double couple
- \( \alpha = 0 \) for a tensional crack
- \( \alpha = 180 \) for a compressional crack
The lune is the set of ordered and normalized eigenvalues.
Moment tensor source types

- $\lambda_3 > 0$
- $\lambda_2 > 0 > \lambda_3$
- $\lambda_1 > 0 > \lambda_2$
- $0 > \lambda_1$
The arc distance on the lune is the minimum angle between moment tensors in matrix space.
If you want to know “how close” a moment tensor is to being a DC (or CLVD or ISO), then measure the arc distance to it.

\[
\cos \theta = \frac{\lambda_1 - \lambda_3}{\sqrt{2} \| \Lambda \|}
\]

Note: here all beachballs have the same frame.

Formula for DC “percentage” from the literature:

\[
c^{DC} = 1 - \frac{2 |\lambda_1 - 2\lambda_2 + \lambda_3| \left| |\lambda_1 + \lambda_2 + \lambda_3| - 3 \max (|\lambda_1|, |\lambda_3|) \right|}{3 \max (|\lambda_1|, |\lambda_3|) \max (|\lambda_1 + \lambda_2 - 2\lambda_3|, |2\lambda_1 - \lambda_2 - \lambda_3|)} - \frac{|\lambda_1 + \lambda_2 + \lambda_3|}{3 \max (|\lambda_1|, |\lambda_3|)}
\]
Moment tensor showing the fault plane in the classical model

\[
M_{pq} = \mu \left( n_p s_q + n_q s_p \right) + \lambda \delta_{pq} S \cdot N
\]

Aki and Richards (1980)

\[
N = Y_{-\alpha/2} e_1 = \left( \cos(\alpha/2), 0, \sin(\alpha/2) \right)
\]

\[
S = Y_{+\alpha/2} e_1 = \left( \cos(\alpha/2), 0, -\sin(\alpha/2) \right)
\]

N and S are fixed for a fixed lune longitude.
The classical model of moment tensors

\[ \hat{\Lambda}(\alpha, \nu) = \frac{1}{\| \|} \left( \frac{\cos \alpha}{1 - 2\nu} + 1, \frac{2\nu \cos \alpha}{1 - 2\nu}, \frac{\cos \alpha}{1 - 2\nu} - 1 \right) \]
Subset of moment tensors with fixed Poisson ratio

As lune longitude increases from left to right, so does the angle between fault and slip vectors, from tensional crack ($\alpha = 0$), to DC ($\alpha = 90$), to compressional crack ($\alpha = 180$).
Subset of crack tensors
Subset of (tensional) crack tensors
From the basic crack-plus-double-couple model (Minson et al., 2007), we can derive an orthogonal measure of the “crack fraction” in any moment tensor.

\[ M^h(\zeta, \phi) = (\cos \zeta) \, D + (\sin \zeta) \, K(\phi) \]

A key point is that \( D \) and \( K \) do not have the same frame.
Estimating a moment tensor involves fitting time-shifted synthetic seismograms to observed seismograms.

Example waveform fits for HOYA nuclear explosion periods 6 – 33 s (red = synthetics, black = data)
The lune can be used to examine the misfit function in the space of model parameters.

Example: HOYA nuclear explosion
The lune can be used to examine source types from different events.

Example: induced events

Tape and Tape (2013) Figure S14
Ford et al. (2010):
“However, as one moves away from the center of the source-type plot (location of a DC mechanism), source orientation becomes less important to the seismic radiation so that the top and bottom of the plot are uniquely represented by an explosion or implosion, respectively (Hudson et al., 1989). A more appropriate population of synthetic sources would take into account the variable degrees of freedom represented in the source-type plot so that source types near the edges of the plot would not have the same density of orientations as those in the center.”
\[ G(u, v, \kappa, \sigma, h) = F(\beta(u), \gamma(v), \kappa, \sigma, \theta(h)) \]
\[ = [\Lambda(\beta(u), \gamma(v))] \hat{U}_{(\kappa, \sigma, \theta(h))} \]
Uniform distribution for 1D (circle) and 2D (sphere) analogs
EXAMPLE: A favorable and a more favorable confidence curve

\( n = 1 \)

\( n = 5 \)

\( \mathbb{P}(\omega) \)

\( \hat{V}(\omega) \)

\( \omega^*(V) \)

\( S^2 \)
Silwal and Tape (2016)
EXAMPLE: Reference tensor at $M = \max(p)$ and $-M$

(a) $m$ at north pole

(b) $m$ at south pole

\[ \mathcal{P}(V) \]

\[ P_{AV} = 6/7 \]

\[ P_{AV} = 1/7 \]

\[ \hat{P}'(\omega) \]

\[ \hat{V}'(\omega) \]

\[ \hat{P}'(\omega) \]

\[ \hat{V}'(\omega) \]
EXAMPLE: Multi-modal probability density
EXAMPLE: Reference tensor has low probability density, but confidence is favorable.
The uniform distribution of moment tensors will depend on the subset.

(a) all moment tensors ($S^5$)
(b) fixed source type (double couple)
(c) fixed source type (non-double couple)
\[ M = [\Lambda] \mathbb{U}, \quad \beta = 90^\circ, \quad \gamma = -10^\circ \]
\[ M = [\Lambda]_{ij}, \quad \beta = \pi/2, \quad \gamma = 0 \]

\[ \Lambda = \Lambda^D \]

\[ \hat{\mathcal{V}}_\Lambda'(\omega) \]
Uniform distribution of moment tensors: evolution from fixed source type (top) to all source types (bottom)
Uncertainty analysis for the case of an assumed double couple moment tensor
High Confidence

Silwal and Tape (2016)
How is source complexity of an explosion imprinted onto the moment tensor?
How is structural complexity imprinted onto the moment tensor?

Homogenized moment tensor and the effect of near-field heterogeneities on nonisotropic radiation in nuclear explosion

Gaël Burgos$^{1,2}$, Yann Capdeville$^3$, and Laurent Guillot$^1$
Source mechanisms change as well pressure changes

Baig and Urbancic (2010)
Final remarks

1. The eigenvalue space of moment tensors (the lune) provides a useful framework for understanding and interpreting full moment tensors and for characterizing uncertainties.

2. Choices in the misfit function are extremely important (bandpass, time windows, allowable time shifts, etc).

3. Fundamental challenge: to interpret moment tensor in physical terms (e.g., oblique opening crack, basic crack-plus-double-couple, two-process model, etc)

download moment tensor scripts on github (feedback welcome):
https://github.com/carltapecompearth

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THANK YOU FOR YOUR ATTENTION!