Mixing Hot and Cold with Sound

$\mathsf{Greg}\ \mathsf{Chini}^\dagger$

Jacques Abdul-Massih[†] Guillaume Michel[‡] Tom Dreeben[§]

[†]Program in Integrated Applied Mathematics and Department of Mechanical Engineering, University of New Hampshire

[‡]Institut Jean Le Rond d'Alembert, Sorbonne Université, CNRS

[§]Central Research Laboratory, Osram Sylvania

IPAM Workshop: Transport and Mixing in Complex/Turbulent Flows January 13th, 2021

GPC and GM gratefully acknowledge support from the Woods Hole Summer Program in Geophysical Fluid Dynamics.

Introduction

Wave-Driven Mean Flows





Steady streaming refers to time-averaged Eulerian flows that arise in periodically forced fluid systems, leading to: water-wave induced sediment transport; winds in equatorial stratosphere; and even circulation of cerebro-spinal fluid in spinal canal!

Acoustic streaming is a technologically important form of steady streaming in which oscillatory driving is provided by high-frequency sound waves

- Eckart streaming: depends on viscous dissipation of waves in body of fluid
- Rayleigh streaming: driven in Stokes boundary layers adjacent to solid walls

Decomposing into time-mean $\overline{(\cdot)}$ and a fluctuation $(\cdot)'$, it can be shown under fairly general circumstances¹ that:

• If fluctuating flow is irrotational ($\omega' \equiv \mathbf{0}$):

$$\bar{\rho}\,\overline{\mathbf{u}'\cdot\nabla\mathbf{u}'}\,=\,\nabla\left(\frac{\bar{\rho}}{2}\overline{|\mathbf{u}'^2|}\right)$$

Induces (or modifies) mean pressure gradient, not streaming

¹Eckart streaming is an exception!

Classical Acoustic Streaming

Rayleigh Streaming (Lord Rayleigh, 1884)



- (i) Small-amplitude standing acoustic waves: $\epsilon \equiv u_*/(\omega\lambda) \ll 1$
- (ii) Thin geometry $h/\lambda \ll 1$
- (iii) Reynolds stress divergence in viscous boundary layer (BL) drives mean flow
- (iv) Mean flow finite at edge of BL:

$$rac{ar{u}}{u_*}|_{y
ightarrow 0^+}\sim -(3\epsilon/4)\overline{u'\partial_{x}u'}=O(\epsilon)$$

Attributes of Rayleigh streaming:

- Intensity: streaming flow outside BL is $O(\epsilon)$ relative to oscillating flow, implying strictly one-way coupling (i.e. waves can be computed as if streaming absent)
- **Pattern:** counter-rotating cells, stacked in the wall-normal direction, and at edge of BL, streaming is directed toward velocity nodes of standing acoustic wave

Technological Applications of Acoustic Streaming

- Microfluidic pumping, mixing, particle capture
- Disruption of dendrites in lithium batteries
- Activated irrigation in medical procedures

Eckart Streaming



• Micro-g heat transfer

 Control of high-intensity discharge (HID) lamps

Rayleigh Streaming



Inapplicability of Classical Rayleigh Theory: Motivating Application-HID Lamps



Dreeben & Chini (2011)² investigated acoustic streaming in high-intensity discharge (HID) lamps, showing that classical Rayleigh streaming theory *not* relevant...

HID Streaming	Rayleigh Theory
0.5 m/s	0.005 m/s
Away from velocity nodes	Toward velocity nodes

²Dreeben, T. D. & Chini, G. P. 2011. 2D streaming flows in high-intensity discharge lamps. *Phys. Fluids* 23, 056101.

Non-Classical Acoustic Streaming

Profound Effect of Background Temperature Gradient



Lin & Farouk (2008)³ performed DNS of full compressible Navier–Stokes equations to investigate impact of acoustic streaming on heat transfer in channels

³Lin, Y. & Farouk, B. 2008. Heat transfer in a rectangular chamber with differentially heated horizontal walls: Effects of a vibrating sidewall. *Int. J. Heat Mass Transfer* **51**, 3179–3189.

Profound Effect of Background Temperature Gradient



Lin & Farouk (2008)⁴ performed DNS of full compressible Navier–Stokes equations to investigate impact of acoustic streaming on heat transfer in channels

Their simulations confirm that character of Rayleigh streaming – both intensity and pattern – is fundamentally altered by imposed (mean) temperature gradient

⁴Lin, Y. & Farouk, B. 2008. Heat transfer in a rectangular chamber with differentially heated horizontal walls: Effects of a vibrating sidewall. Int. J. Heat Mass Transfer **51**, 3179–3189.

Baroclinic Acoustic Streaming



Fluctuating vorticity produced baroclinically rather than by viscous torques!

$$\bar{\rho}\partial_t \mathbf{u}' pprox - \nabla p' \quad \Rightarrow \quad \partial_t \left(\nabla \times \mathbf{u}'
ight) pprox rac{
abla ar{
ho} \times
abla p'}{ar{
ho}^2}$$

Chini, Malecha & Dreeben (2014)⁵ demonstrated the potential for *strong* baroclinically-driven acoustic streaming

⁵Chini, G. P., Malecha, Z. & Dreeben, T. D. 2014. Large-amplitude acoustic streaming. J. Fluid Mech. 744, 329–351.

Problem Formulation



<u>BCs</u>: $u = V = \Theta = 0$ $T = T_B(Y) + \Theta(x, Y, t)$ where background temperature:

 $T_B(Y) = 1 + \Gamma Y$

Note: Buoyancy forces neglected

Problem Formulation



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Compressible NS Equations

whe

$$\rho \left[\partial_t u + (\mathbf{u} \cdot \nabla) \, u \right] = -\frac{1}{\gamma} \partial_x \pi + \frac{1}{Re_w} \left[\nabla^2 u + \frac{1}{3} \partial_x \left(\nabla \cdot \mathbf{u} \right) \right]$$
$$\rho \left[\partial_t V + (\mathbf{u} \cdot \nabla) \, V \right] = -\frac{1}{\delta^2 \gamma} \partial_Y \pi + \frac{1}{Re_w} \left[\nabla^2 V + \frac{1}{3\delta^2} \partial_Y \left(\nabla \cdot \mathbf{u} \right) \right]$$
$$\partial_t \rho + \partial_x (\rho u) + \partial_Y (\rho V) = 0$$
$$\partial_t \Theta + (\mathbf{u} \cdot \Theta) + V \frac{dT_B}{dY} = (1 - \gamma) (T_B + \Theta) (\nabla \cdot \mathbf{u}) + \frac{\gamma}{\rho Pr Re_w} \nabla^2 \Theta$$
$$1 + \pi = \rho (T_B + \Theta)$$
re $\mathbf{u} = (u, \delta V)$ and $\nabla (\cdot) = [\partial_x (\cdot), \frac{1}{\delta} \partial_Y (\cdot)]$

Dimensionless Parameters, Distinguished Limit & Multiple Scale (WKBJ) Analysis

Parameter	Definition	Scaling
Wave Amplitude ϵ	$k_*u_*/\omega_* = u_*/a_*$	$\epsilon \ll 1$
Aspect Ratio δ	k_*H_*	$\delta \equiv \epsilon^{1/2} h$
Temperature Gradient F	$\Delta \Theta_*/T_*$	$\Gamma = O(1)$
Reynolds Number <i>Re</i> w	$a_*/k_* u_*$	$Re_w \equiv \epsilon^{-2}R$
Prandtl Number <i>Pr</i>	$ u_*/\kappa_* $	Pr = O(1)
Specific Heat Ratio γ	c_p/c_v	$\gamma = O(1)$

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WKBJ analysis to capture fast and slow evolution, using phase variable $\phi(t) \equiv \Phi(T)/\epsilon$ and slow time scale $T \equiv \epsilon t$, where the slowly-varying frequency $\omega = -\partial_T \Phi$:

$$f(x, Y, t; \epsilon) = \overline{f}(x, Y, T; \epsilon) + f'(x, Y, \phi; T, \epsilon)$$

Asymptotic expansions for various fields:

$$\begin{bmatrix} u, V, \pi \end{bmatrix} \sim \epsilon [\bar{u}_1 + u'_1, \bar{V}_1 + V'_1, \pi'_1] + \epsilon^2 [\bar{u}_2 + u'_2, \bar{V}_2 + V'_2, \bar{\pi}_2 + \pi'_2] + \dots \\ \begin{bmatrix} \Theta, \rho \end{bmatrix} \sim [\bar{\Theta}_0, \bar{\rho}_0] + \epsilon [\bar{\Theta}_1 + \Theta'_1, \bar{\rho}_1 + \rho'_1] + \dots$$

Asymptotic Analysis

Leading-Order, Quasilinear (QL) Wave/Mean-Flow System

Streaming Flow

$$\begin{split} \bar{\rho}_{0} \left(\partial_{T} \bar{u}_{1} + \bar{u}_{1} \partial_{x} \bar{u}_{1} + \bar{V}_{1} \partial_{Y} \bar{u}_{1} \right) &+ \frac{1}{\gamma} \partial_{x} \bar{\pi}_{2} &= -\partial_{x} \left(\bar{\rho}_{0} \overline{u_{1}'^{2}} \right) - \partial_{Y} \left(\bar{\rho}_{0} \overline{u_{1}' V_{1}'} \right) + \frac{1}{Rh^{2}} \partial_{Y}^{2} \bar{u}_{1} \\ \partial_{Y} \bar{\pi}_{2} &= 0 \\ \partial_{x} \bar{u}_{1} + \partial_{Y} \bar{V}_{1} &= \frac{1}{PrRh^{2}} \partial_{Y}^{2} \Theta \\ \partial_{T} \bar{\Theta}_{0} + \bar{u}_{1} \partial_{x} \bar{\Theta}_{0} + \bar{V}_{1} \left(\partial_{Y} \bar{\Theta}_{0} + \frac{dT_{B}}{dY} \right) &= (1 - \gamma)(T_{B} + \bar{\Theta}_{0})(\partial_{x} \bar{u}_{1} + \partial_{Y} \bar{V}_{1}) \\ \bar{\rho}_{0} \left(T_{B} + \bar{\Theta}_{0} \right) = 1 &+ \left(\frac{\gamma}{PrRh^{2}} \right) \frac{1}{\bar{\rho}_{0}} \partial_{Y}^{2} \bar{\Theta}_{0} \end{split}$$

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Acoustic Waves

$$\begin{split} \omega_0\bar{\rho}_0\partial_\phi u_1' &= -\frac{1}{\gamma}\partial_x\pi_1'\\ \partial_Y\pi_1' &= 0\\ \omega_0\partial_\phi\rho_1' + \partial_x\left(\bar{\rho}_0u_1'\right) + \partial_Y\left(\bar{\rho}_0V_1'\right) &= 0\\ \omega_0\partial_\phi\Theta_1' + u_1'\partial_x\bar{\Theta}_0 + V_1'\left(\partial_Y\bar{\Theta}_0 + \frac{dT_B}{dY}\right) &= (1-\gamma)(T_B + \bar{\Theta}_0)(\partial_xu_1' + \partial_YV_1')\\ \pi_1' &= \rho_1'(T_B + \bar{\Theta}_0) + \bar{\rho}_0\Theta_1' \end{split}$$

Leading-Order, Quasilinear (QL) Wave/Mean-Flow System

Streaming Flow

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Acoustic Waves

$$\partial_{x}\left[\left(\frac{1}{\overline{\rho}_{0}}\right)\partial_{x}\pi_{1}'\right] + \partial_{Y}\left[\left(\frac{1}{\overline{\rho}_{0}}\right)\partial_{Y}\pi_{1}'\right] = \omega_{0}^{2}\partial_{\phi}^{2}\pi_{1}'$$

NOTE: Stokes layers are passive.

Elimination of Fast Acoustic Wave Dynamics. I. Mode Structure

Quasilinear (QL) structure of wave equations enables linear WKBJ ansatz, i.e.

$$f_1'(x,Y,\phi;T) = A(T) \left[\hat{f}_1(x,Y;ar{
ho}_0) e^{i\phi} + c.c.
ight]$$

2D non-separable partial differential eigenvalue problem for \hat{f}_1 can be simplified:

$$\hat{u}_1(x,Y;\bar{\rho}_0) = -\frac{g'(x;\bar{\rho}_0)}{\omega_0^2\bar{\rho}_0(x,Y,T)} \qquad \hat{v}_1(x,Y;\bar{\rho}_0) = Yg(x;\bar{\rho}_0) + \partial_x \left(\frac{g'(x;\bar{\rho}_0)}{\omega_0^2} \int_0^Y \frac{\mathrm{d}Y}{\bar{\rho}_0}\right)$$

where g(x) and $\omega_0 = \partial_T \Phi$ satisfy the **1D** e-value problem

$$g^{\prime\prime}(x)+\frac{\alpha^{\prime}(x)}{\alpha(x)}g^{\prime}(x)+\frac{\omega_{0}^{2}}{\alpha(x)}g(x)=0, \text{ where } \alpha(x)=\int_{0}^{1}\frac{\mathrm{d}Y}{\bar{\rho}_{0}} \text{ and } g^{\prime}(0)=g^{\prime}(2\pi)=0$$

with normalization condition $\int_0^{2\pi} g^2(x; \bar{\rho}_0) dx = 1$.

Elimination of Fast Acoustic Wave Dynamics. II. Modal Amplitude

Novel amplitude equation obtained by extending analysis of waves to higher order:

$$\begin{aligned} \frac{2}{A\omega_0^{-1}} \frac{\mathrm{d}(A\omega_0^{-1})}{\mathrm{d}T} &= -\frac{i\omega_0}{Pe_s h^2} \int \mathrm{d}x \mathrm{d}Y \, g \partial_Y^2 \hat{\Theta}_1 + \frac{1}{2\omega_0^2} \int \mathrm{d}x \mathrm{d}Y \, g'^2 \left(\bar{u}_1 \partial_x \bar{\rho}_0^{-1} + \bar{v}_1 \partial_Y \bar{\rho}_0^{-1}\right) \\ &+ \int \mathrm{d}x \mathrm{d}y (\partial_x \bar{u}_1 + \partial_y \bar{v}_1) \left[(\gamma + 1)g^2 + 2i\omega_0 \hat{\Theta}_1 g \bar{\rho}_0 + \frac{g'^2}{\omega_0^2 \bar{\rho}_0} \left(Pr - \frac{1}{2} \right) \right] \end{aligned}$$

• May be interpreted as slow-time energy balance for acoustic wave, since

$$\overline{E}_1 \equiv \frac{1}{2} \int_0^{2\pi} \mathrm{d}x \int_0^1 \mathrm{d}Y \bar{\rho}_0 \overline{u_1'^2} = \left(\frac{A(T)}{2\omega_0}\right)^2 \quad \Rightarrow \quad \frac{2}{A\omega_0^{-1}} \frac{\mathrm{d}(A\omega_0^{-1})}{\mathrm{d}T} = \frac{1}{\overline{E}_1} \frac{\mathrm{d}\overline{E}_1}{\mathrm{d}T}$$

 Derivation requires proper accounting of variation of eigenfunctions with slow time owing to their functional dependence on p
₀(x, Y, T)

Virtue of approach is that computations can be performed strictly on slow time scale of streaming flow by time-advancing mean + amplitude equations and, each slow-time step, solving eigenvalue problem for wave frequency and mode structure.

Weak Streaming: 1-Way Coupling

Parameters corresponding to Lin & Farouk (2008) DNS... $\epsilon = 10^{-2}$, $\gamma = 1.4$, Pr = 0.71, h = 2.3, $\Gamma = 0.2$, R = 5.7, $A \approx 6$

Acoustic Wave Velocity Field



Weak Streaming: 1-Way Coupling



Acoustic Wave Velocity Field



Weak Streaming: Quantitative Comparison w/Lin & Farouk (2008)

No fitting parameters... $\epsilon = 10^{-2}$, $\gamma = 1.4$, Pr = 0.71, h = 2.3, $\Gamma = 0.2$, R = 5.7, $A \approx 6$

Weak Streaming: Quantitative Comparison w/Lin & Farouk (2008)

 $\epsilon = 10^{-2}, \ \gamma = 1.4, \ \overline{Pr = 0.71, \ h = 2.3, \ \Gamma = 0.2, \ R = 5.7, \ A \approx 6}$



DNS of full (2D) compressible NS equations by Lin & Farouk (2008):

- Included additional physics (e.g. temperature-dependent diffusivities)
- Computationally-expensive... computed only 1 eddy-turnover time!

Finite-Amplitude Streaming: 2-Way Coupling

Slow-flow system solved using *Dedalus* code with constant power \mathcal{P} injection:

 $\frac{1}{\overline{E}_1} \frac{\mathsf{d}\overline{E}_1}{\mathsf{d}T} = \dots + \frac{\mathcal{P}}{\overline{E}_1}$

Using parameters: $\overline{\epsilon} = 10^{-2}, \ \gamma = 1.4, \ Pr = 1, \ h = 4, \ \Gamma = 1, \ R = 4$ $\mathcal{P} = 0.004$

Finite-Amplitude Streaming: 2-Way Coupling

Slow-flow system solved using *Dedalus* code with constant power \mathcal{P} injection:

$$\frac{1}{\overline{E}_1} \frac{\mathsf{d}\overline{E}_1}{\mathsf{d}T} = \dots + \frac{\mathcal{P}}{\overline{E}_1}$$

Using parameters: $\overline{\epsilon} = 10^{-2}, \ \gamma = 1.4, \ Pr = 1, \ h = 4, \ \Gamma = 1, \ R = 4$ $\mathcal{P} = 0.004$



T = 120





T = 10

Summary: Rayleigh vs. Baroclinic Acoustic Streaming

Property	Rayleigh Streaming	Baroclinic Streaming
Relative magnitude	$ar{u}/u_* = O(\epsilon)$	$ar{u}/u_*=O(1)$
Pattern	Stacked cells	Cells span channel
Wave/mean-flow coupling	1-way	2-way
Heat transport	6 Nu $- 1 \propto \epsilon^{2} A^{4} R^{2} h^{2}$	$\mathit{Nu}-1 \propto \mathit{A}^4 \mathit{R}^4 \mathit{h}^8$

⁶Vainshtein, P. Fichman, M. & Gutfinger, G. 1995 Acoustic streaming enhancement of heat transfer between two parallel plates. Int. J. Heat. Mass Transfer, **38**, 1893–1899.

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However, prefactors in (Nu - 1)-Ra relationship are rather small (at least in one-way coupling limit for which scaling result easily derived)...

Increasing Nu by increasing aspect-ratio δ is feasible for baroclinic acoustic streaming.

⁶Vainshtein, P. Fichman, M. & Gutfinger, G. 1995 Acoustic streaming enhancement of heat transfer between two parallel plates. Int. J. Heat. Mass Transfer. 38, 1893–1899.

Ongoing Work: Impact of Aspect Ratio, BCs, Control Parameters on Heat Transfer

• What is aspect-ratio dependence of heat transport?

For finite aspect-ratio [$\delta = O(1)$] case, must repeatedly solve non-separable 2D partial differential eigenvalue problem for wave field:

 $\partial_{x}\left[\overline{\rho}_{0}^{-1}\partial_{x}\hat{\pi}_{1}\right] + \delta^{-2}\partial_{y}\left[\overline{\rho}_{0}^{-1}\partial_{y}\hat{\pi}_{1}\right] = -\omega_{0}^{2}\hat{\pi}_{1}, \text{ where: } \overline{\rho}_{0} = \overline{\rho}_{0}(x, y, T)$

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• Will streaming intensity (and, hence, cooling) be reduced when **interior** temperature/density field is **well mixed**? What if at least one boundary satisfies a **fixed heat flux** rather than fixed temperature condition?



Finite Aspect-Ratio Baroclinic Acoustic Streaming: Turbulent Transport

Finite Aspect-Ratio Baroclinic Acoustic Streaming: Turbulent Transport



Finite Aspect-Ratio Baroclinic Acoustic Streaming: Turbulent Transport



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Finite Aspect-Ratio Baroclinic Acoustic Streaming: Turbulent Transport



Finite Aspect-Ratio Baroclinic Acoustic Streaming: Turbulent Transport



Wave forcing concentrates in streaming thermal boundary layers!



Summary Points and Open Questions

Baroclinic acoustic streaming flows^{7 8}:

- Arise in presence of ambient/imposed transverse temperature/density gradients
- Characterized by velocities that are comparable to acoustic wave motions
- Generically involve two-way coupling between waves and mean flows

Unless temperature differences very small, **cannot** simply couple Rayleigh streaming predictions to appropriate (e.g. heat) transport equation, as in Richardson (1967), Davidson (1973), Vainshtein *et al.* (1995)...

Derived a **novel amplitude equation** that properly incorporates slow changes in eigenfunctions owing to mean-field evolution [cf. Karlsen *et al.* (2016, 2017)]

Open mathematical questions:

- (i) well-posedness of reduced system?
- (ii) rigorous **bounds** on heat transport as function of control parameters?
- (iii) efficient algorithms for 2D eigenvalue problem?

J. Fluid Mech. 858, 536-564.

⁷Michel, G. & Chini, G. P. Strong wave-mean-flow coupling in baroclinic acoustic streaming. 2019.

⁸Nama, N. Mixing hot and cold with sound. 2019. J. Fluid Mech. Focus on Fluids 866, 1–4.