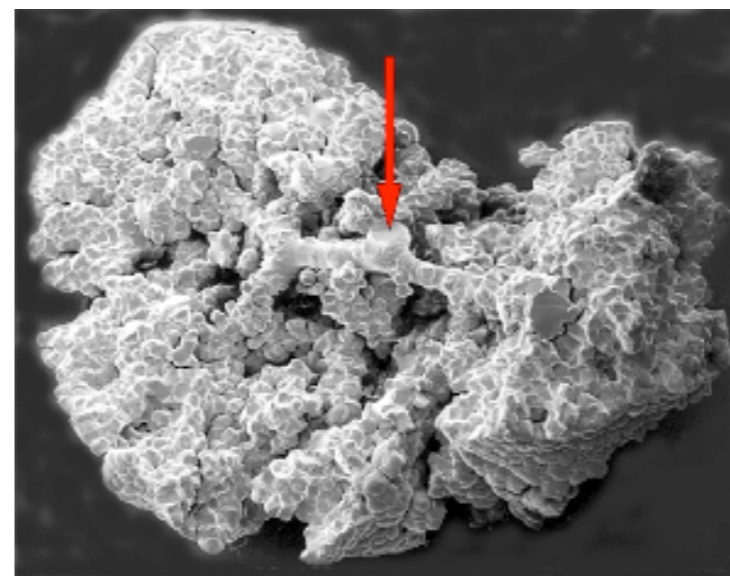
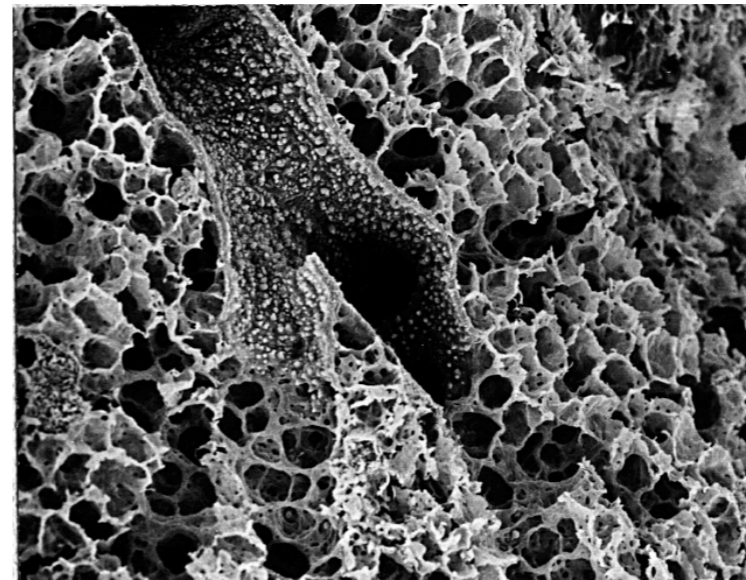
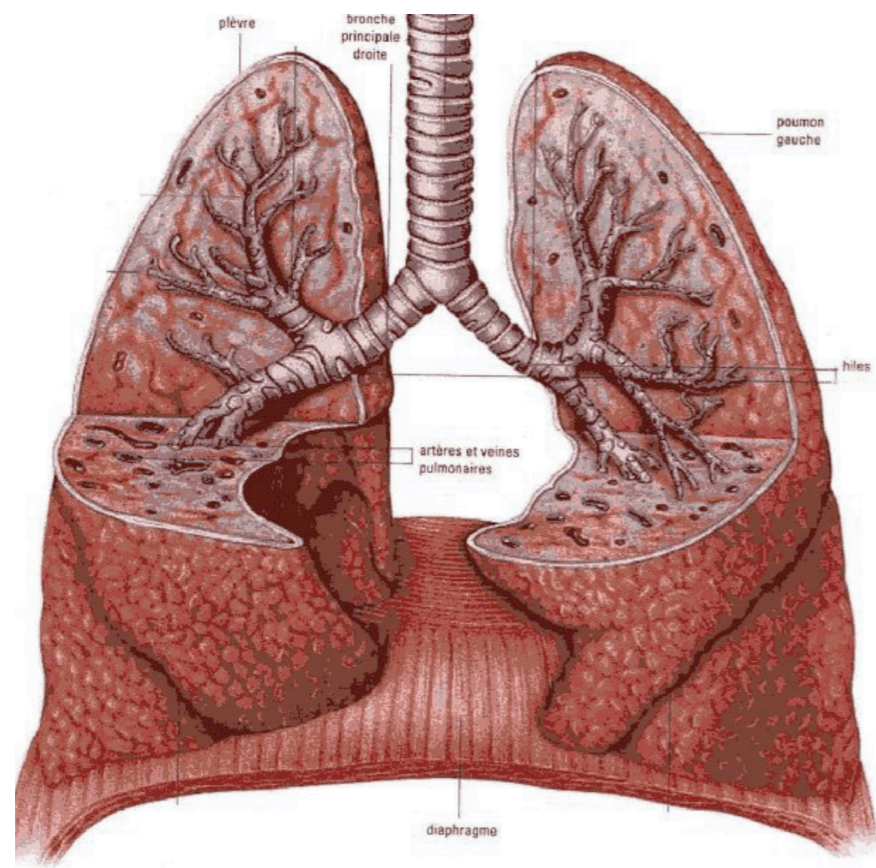


# Multiscale Modeling of the Respiratory System

Céline Grandmont  
Projet REO

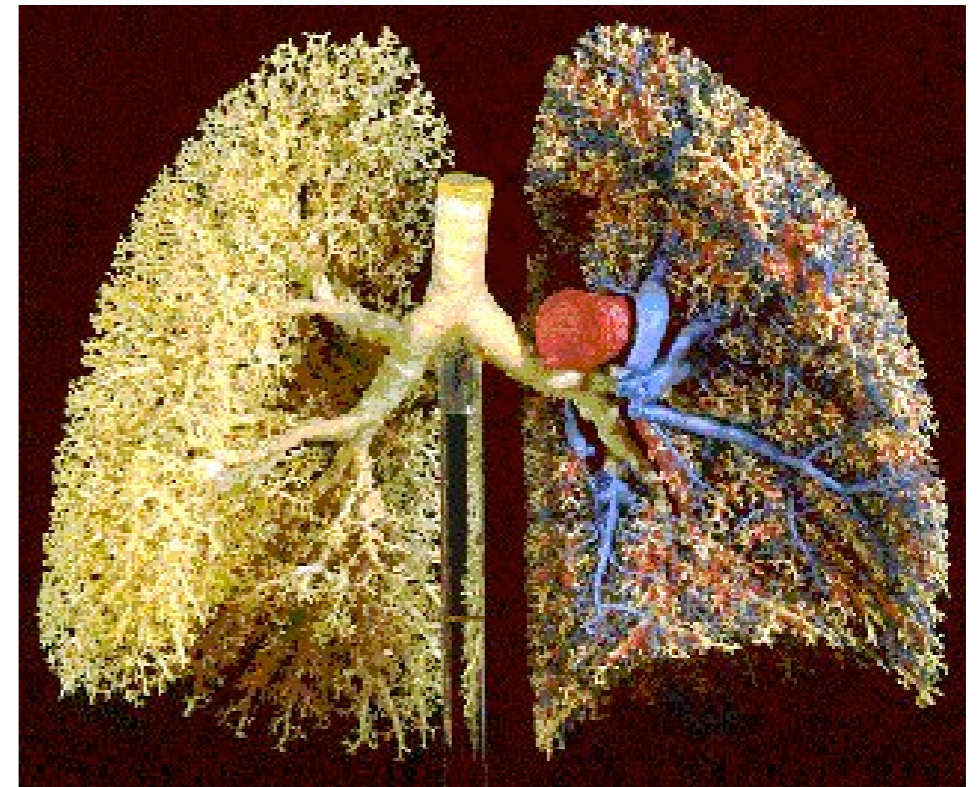


# Respiratory System Structure



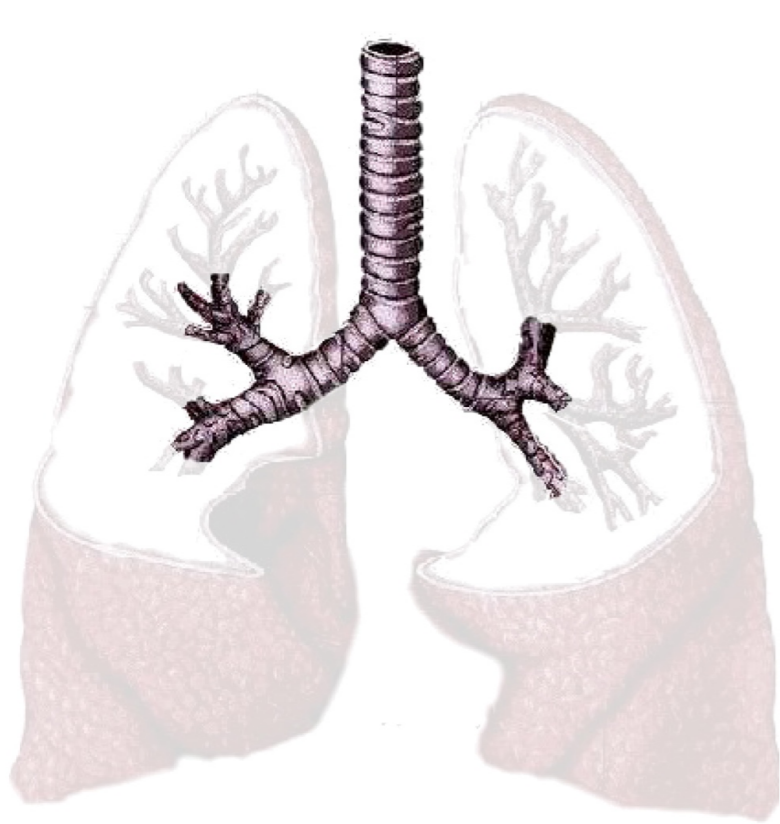
# The Respiratory System

- Enable gas exchanges
- Pathologies:
  - Asthma
  - Fibrosis, emphysema
  - ...



Weibel

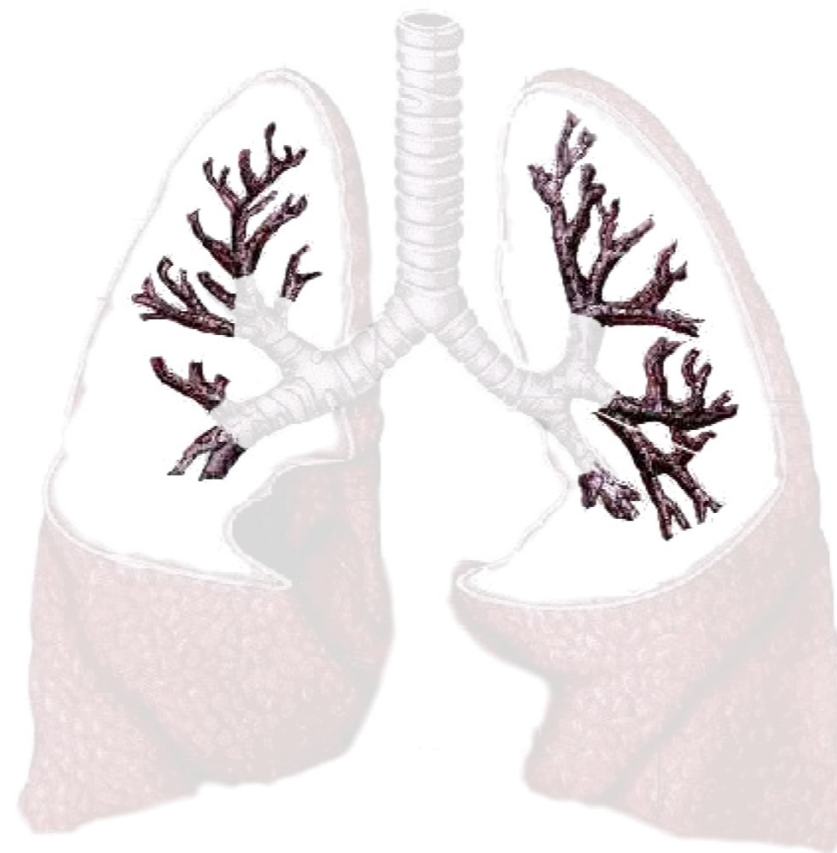
# Multiscale Strategy



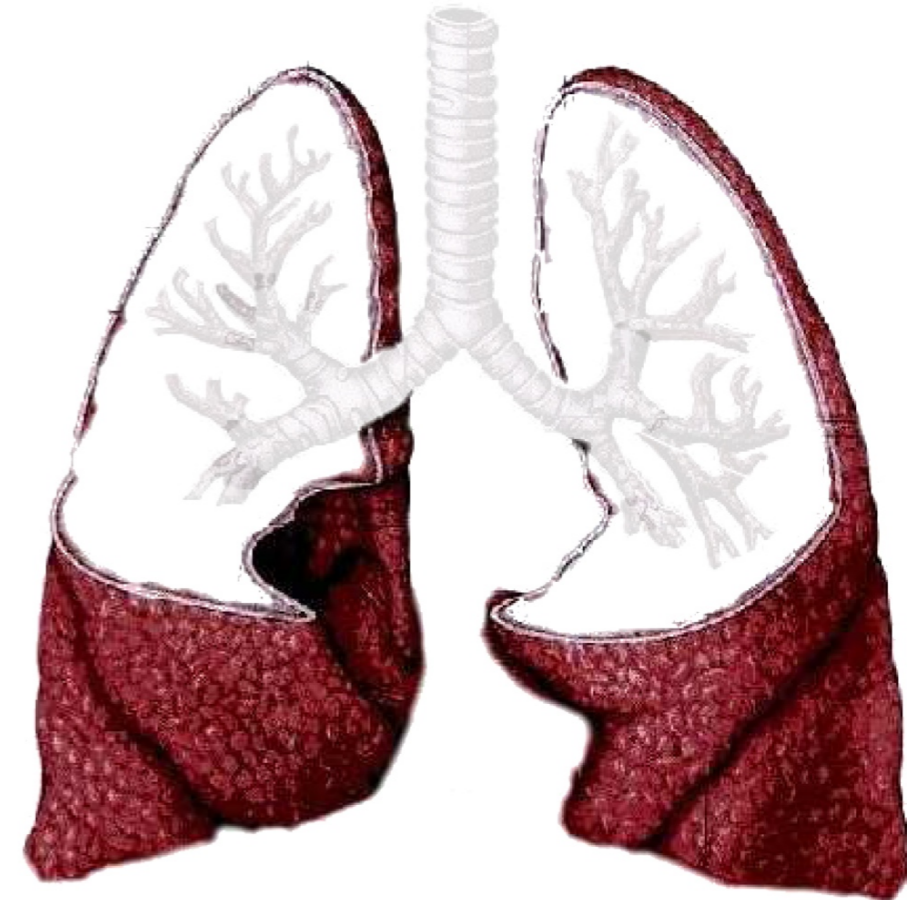
3D modeling

Viscous

incompressible flow



Laminar flow



Simple elastic  
model

# Goals

- Obtain simple but representative models
  - ▶ Modeling each zone ;
  - ▶ Coupling each model ;
  - ▶ or take into account the other parts thanks to well chosen boundary conditions ;

# Outline

- Viscoelastic model of the lung parenchyma  
[CG, Maury, Meunier, Vannier]
- Air flow modeling in the proximal part  
[Baffico, CG, Maury, Soualah]
- Air - Spray modeling  
[Boudin, Desvillettes, Filoche, CG, Moussa]

# Modeling of the lung parenchyma

C.G., B. Maury, N. Meunier

Condensation of the bronchial tree

## Hypothesis

- Diadic tree of pipes
- In each tube the **Poiseuille law** is satisfied  $\implies$  the flow is characterized by a resistance  $r_n$  at each generation

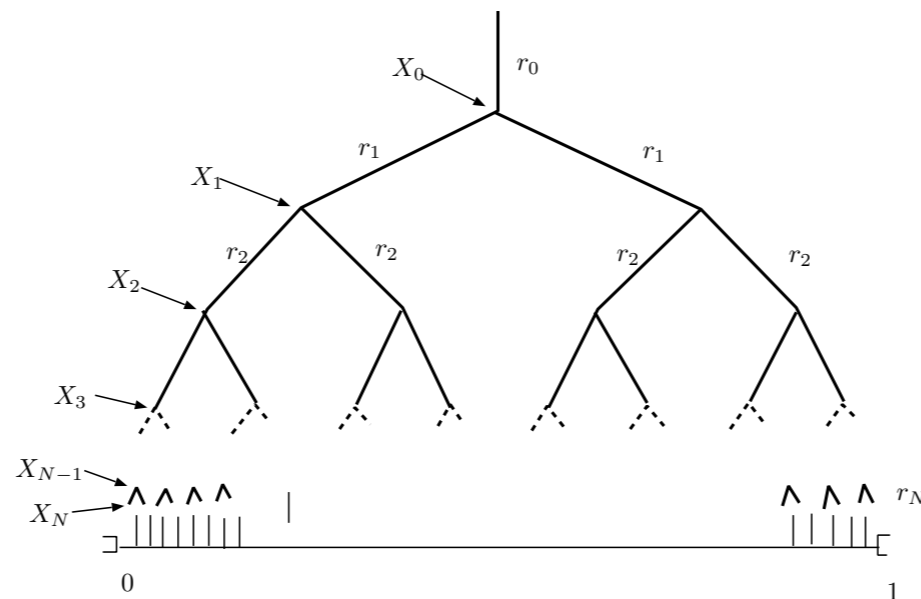


FIGURE 1. Dyadic tree

# Condensation of the bronchial tree

$$p_i = \sum_{j=0}^{2^N - 1} q_j R_{N - \nu_{ij}},$$

with

$$R_n = \sum_{j=0}^n r_j,$$

and

$$\nu_{ij} = \inf\{k \geq 0, \alpha_\ell = \beta_\ell \quad \forall \ell \geq k\},$$

$$i = \sum_{k=0}^{\infty} \alpha_k 2^k, \quad j = \sum_{k=0}^{\infty} \beta_k 2^k \quad \text{with } \alpha_k, \beta_k \in \{0, 1\} \quad \forall k.$$

# Condensation of the bronchial tree

Let  $u \in L^2(I)$ , we define  $2^N$  flux flows

$$\mathbf{q}^N = (q_i^N)_{i=0, \dots, 2^N-1}, q_i^N = \int_{\frac{i}{2^N}}^{\frac{i+1}{2^N}} u(y) dy.$$

To the pressure vector  $\mathbf{p}^N = (p_i^N)_{i=0, \dots, 2^N-1}$ , we associate the function  $p$  that takes the value  $p_i^N$  on  $(\frac{i}{2^N}, \frac{i+1}{2^N})$ .

Then

$$p(x) = \int_I K_N(x, y) u(y) dy, a.e.$$

where  $K_N \in L^1(I \times I)$  is a function piecewise constant and defined by

$$x \in \left(\frac{i}{2^N}, \frac{i+1}{2^N}\right), y \in \left(\frac{j}{2^N}, \frac{j+1}{2^N}\right) \mapsto R_{N-\nu_{ij}}.$$

# Condensation of the bronchial tree

Limit when  $N \rightarrow +\infty$

$$K_N \longrightarrow K, a.e.$$

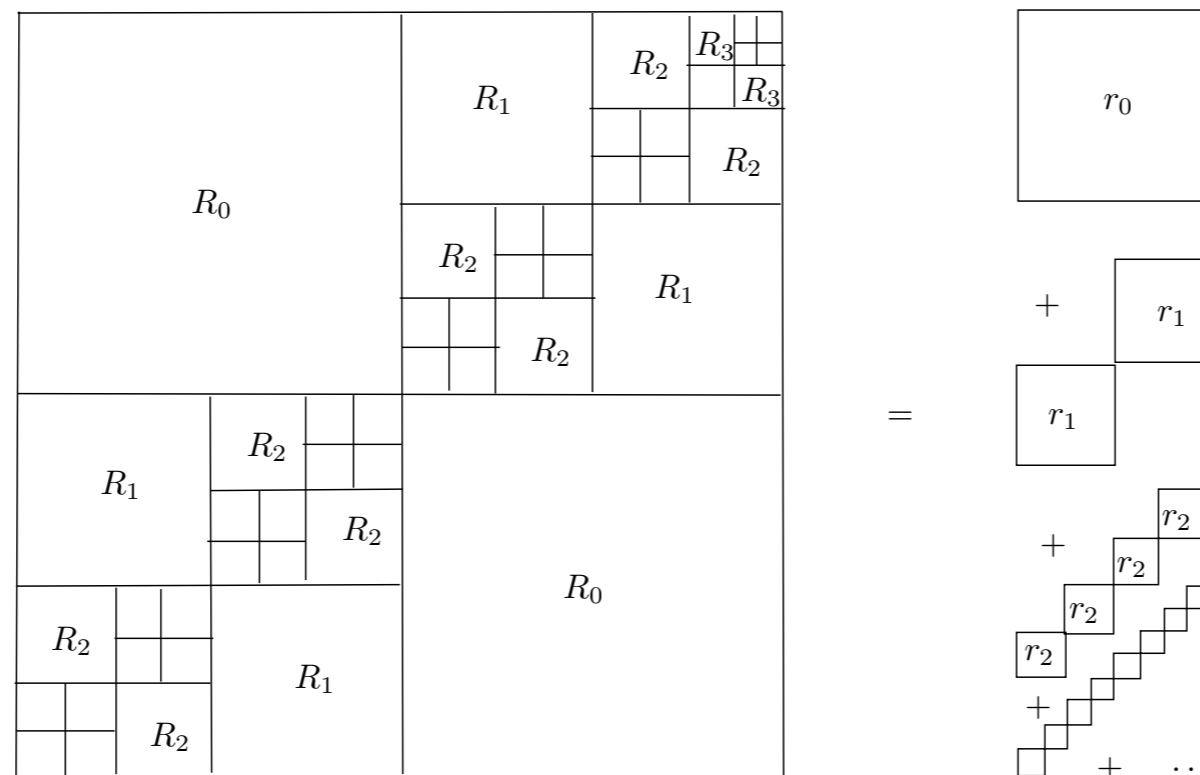


FIGURE 1. Kernel  $K(x, y)$

# Condensation of the bronchial tree

## Properties of the limit operator

- $\mathcal{R}_N \longrightarrow \mathcal{R}$  in  $\mathcal{L}(L^2(I))$  iff  $\sum_{n \geq 0} \frac{r_n}{2^n} < +\infty$ .
- $\|\mathcal{R}_N u\|_{L^p(I)} \leq \|K_N\|_{L^1(I \times I)} \|u\|_{L^p(I)}$ .
- $\mathcal{R}$  self-adjoint, compact, monotone.
- The Haar basis is a family of eigenfunctions of  $\mathcal{R}$  associated to the eigenvalues  $\lambda_N = \sum_{n=N}^{+\infty} \frac{r_n}{2^n}$ .
- if  $\sum_{n \geq 0} \frac{r_n}{2^n} = +\infty$  then  $\int_I \frac{K_N(\cdot, y)}{\|K_N\|_{L^1(I \times I)}} q(y) dy \longrightarrow q(\cdot)$ .

# Condensation of the bronchial tree

## Geometric Tree

We consider the case  $r_n = r_0 \alpha^n$ . [Human lung:  $\alpha = 1.63$ ]

- $\mathcal{R}_N \longrightarrow \mathcal{R}$  in  $\mathcal{L}(L^2(I))$  if  $\alpha < 2$ .

- if  $\alpha = 2$  then  $\int_I \frac{K_N(\cdot, y)}{\|K_N\|_{L^1(I \times I)}} q(y) dy \longrightarrow q(\cdot)$ .

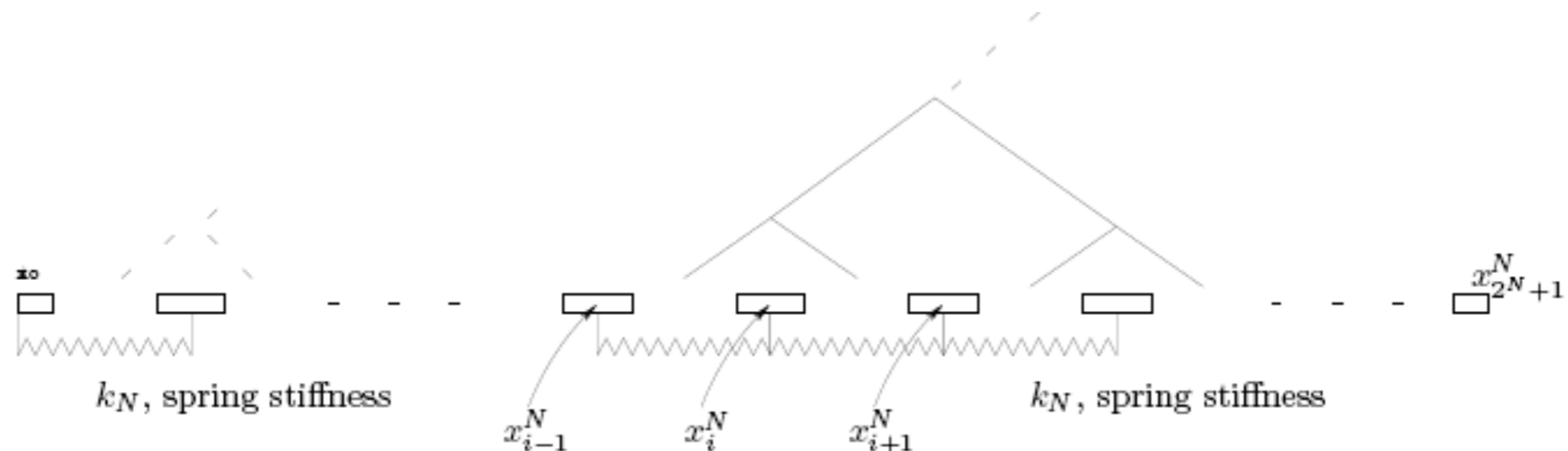
Remark:  $\alpha = 2$  corresponds to an optimal coefficient that is the minimizer of the global resistance under a volume constrain.

[B. Mauroy, M. Filoche, E. R. Weibel, B. Sapoval]

# Viscoelastic model

## Spring-mass system

We consider a succession of masses (lung parenchyma) and of air pockets (alveoli), each mass being linked by springs. Thus each air pocket is connected to each other through the tree.



# Viscoelastic model

## Spring–mass sytem

The motion of the  $i - th$  mass is described by:

$$m_N \ddot{u}_i^N(t) - k_N (u_{i+1}^N(t) - 2u_i^N(t) + u_{i-1}^N(t)) + p_i^N(t) - p_{i-1}^N(t) = m_N f_i^N(t),$$

with

$$p_i^N = \sum_{j=0}^{2^N - 1} R_{N-\nu_{ij}} q_j^N,$$

and

$$q_j^N = \dot{u}_j^N(t) - \dot{u}_{j+1}^N(t).$$

# Viscoelastic model

## *A priori* Estimates

$(u^N)$  is bounded in  $W^{1,\infty}(0, T; L^2(0, 1)) \cap L^\infty(0, T; H_0^1(0, 1))$ .

Limit equation in the case  $\sum \frac{r_n}{2^n} < +\infty$

$$\rho \alpha_s \partial_{tt} u(x, t) - k \partial_{xx} u(x, t) - \partial_x \int_0^1 K(x, y) \partial_y \partial_t u(y, t) dy = \rho \alpha_s f(x, t),$$

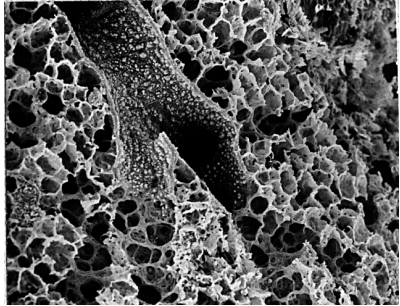
where  $k$  satisfies:

$$k = \frac{k_N}{2^N}.$$

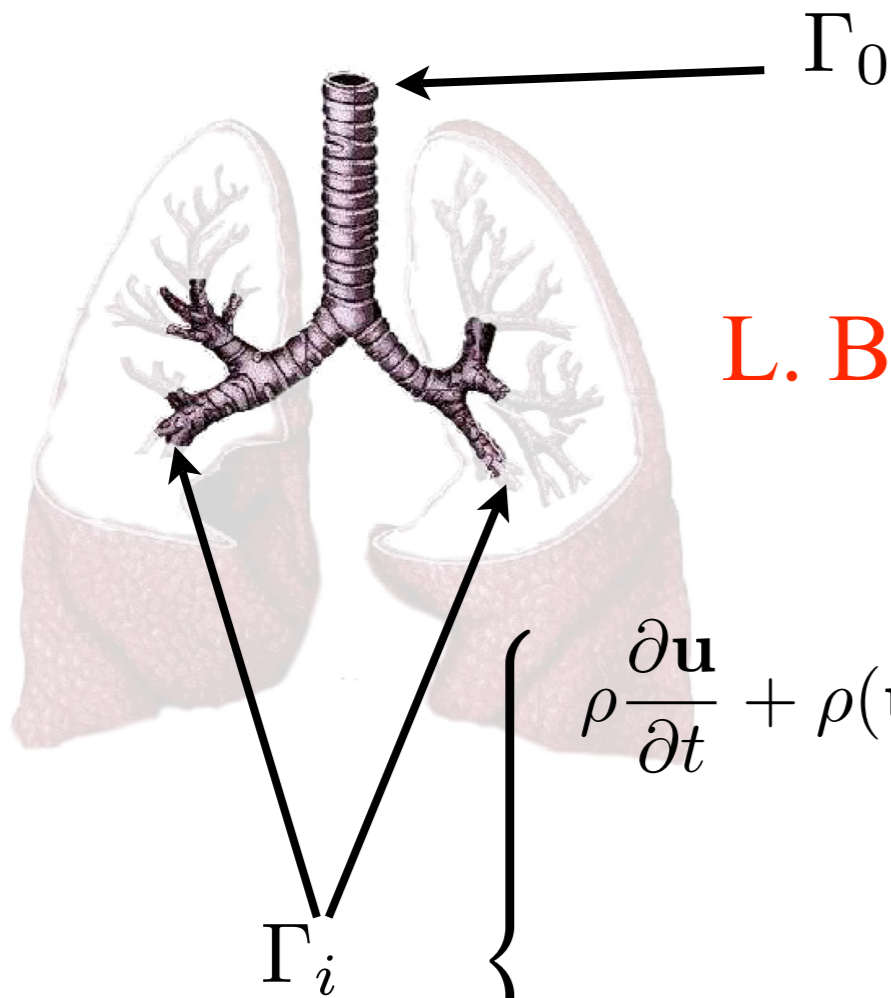
Limit in the case  $\sum \frac{r_n}{2^n} = +\infty$

$u = u_0$ , where  $u_0$  is the initial displacement.

# Ongoing and Related Works

- L. Baffico, C. G., Y. Maday, A. Osses, Homogenized foam model; 
- C.G., C. Vannier, long time behavior;
- B. Maury, D. Salort, C. Vannier, diadic tree;
- Y. Achdou, C. Sabot, N. Tchou, boundary conditions for self similar geometries.

# Air flow in the proximal part



L. Baffico, C. G., Y. Maday B. Maury, A. Soualah

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho(\mathbf{u} \cdot \nabla) \mathbf{u} - \mu \Delta \mathbf{u} + \nabla p = 0, \quad \text{in } \Omega,$$

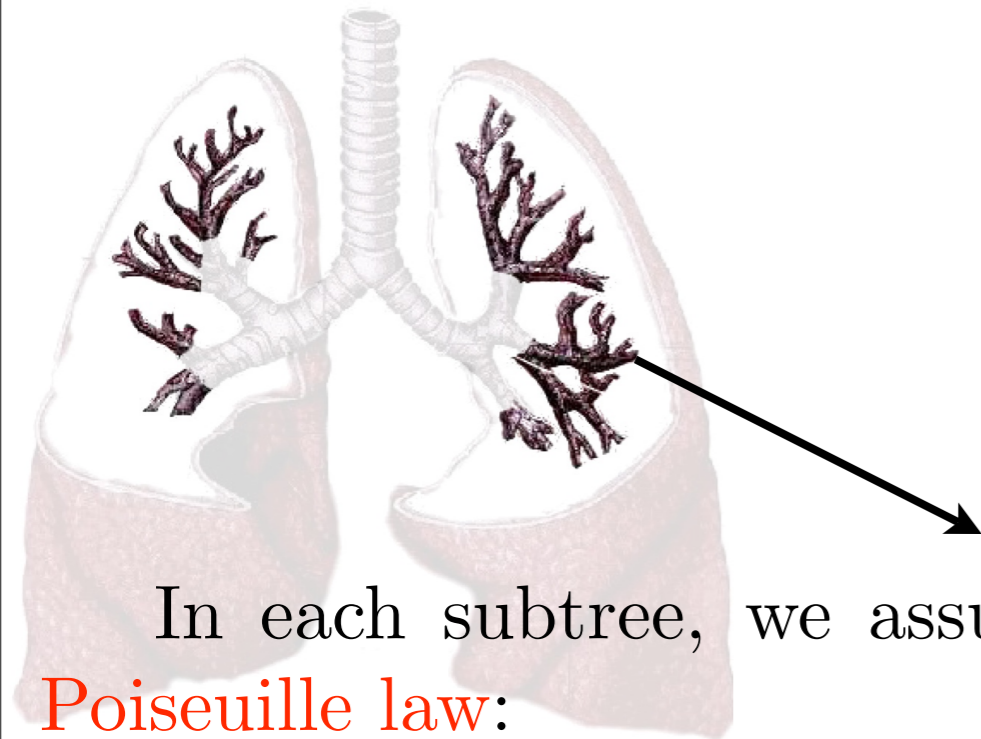
$$\nabla \cdot \mathbf{u} = 0, \quad \text{in } \Omega,$$

$$\mathbf{u} = 0, \quad \text{on } \Gamma_l,$$

$$\mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} = -P_0 \mathbf{n} \quad \text{on } \Gamma_0,$$

$$\mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} = -\Pi_i \mathbf{n} \quad \text{on } \Gamma_i \quad i = 1, \dots, N,$$

# Air flow in the distal part



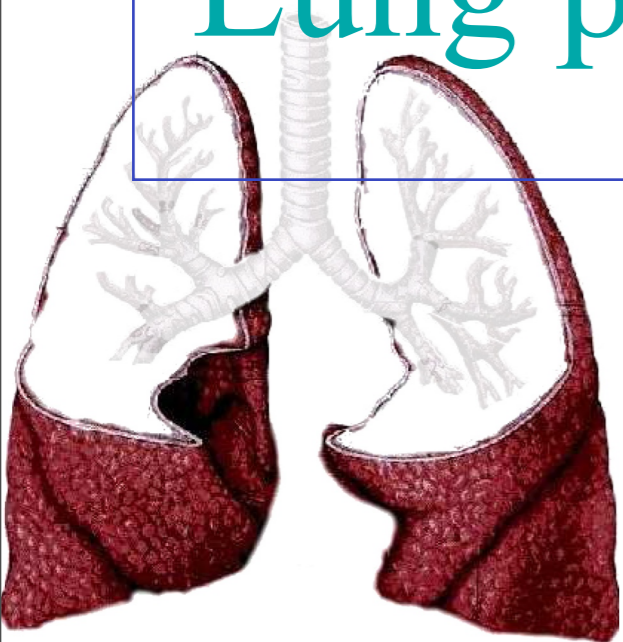
In each subtree, we assume that the flow is **laminar** and thus satisfies a **Poiseuille law**:

$$\Pi_i - P_i = R_i \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n}, \quad R_i \geq 0,$$

where  $R_i$  denotes the equivalent resistance of the distal tree and  $P_i$  is an alveola pressure. The boundary conditions at the outlets  $\Gamma_i$  writes

$$\mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} = -P_i \mathbf{n} - R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \mathbf{n} \quad \text{on } \Gamma_i \quad i = 1, \dots, N.$$

# Lung parenchyma - Diaphragm muscle



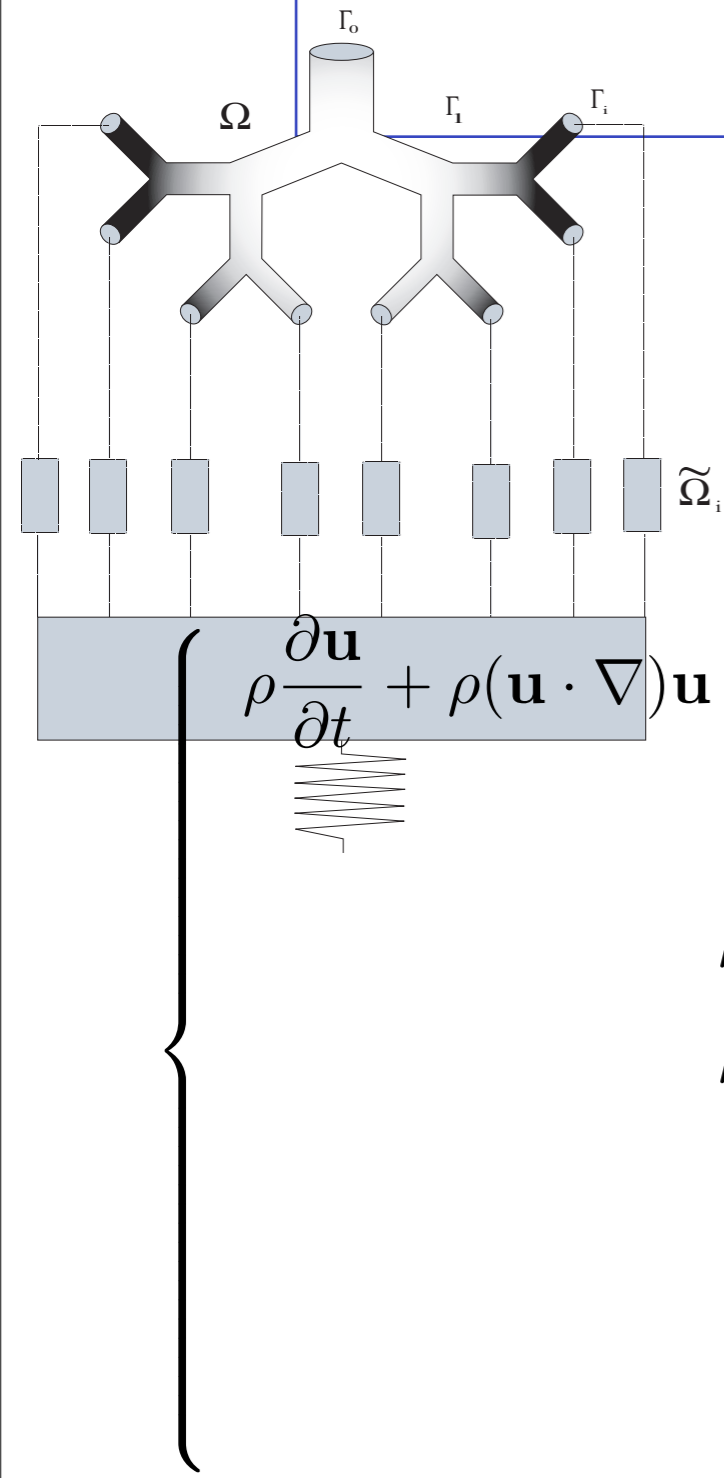
All the alveola pressures are equal:  $P_i = P_a$ . The diaphragm and parenchyma motion are govern by:

$$m\ddot{x} = -kx + f_{ext} + SP_a,$$

Moreover, since the flow and the parenchyma are incompressible

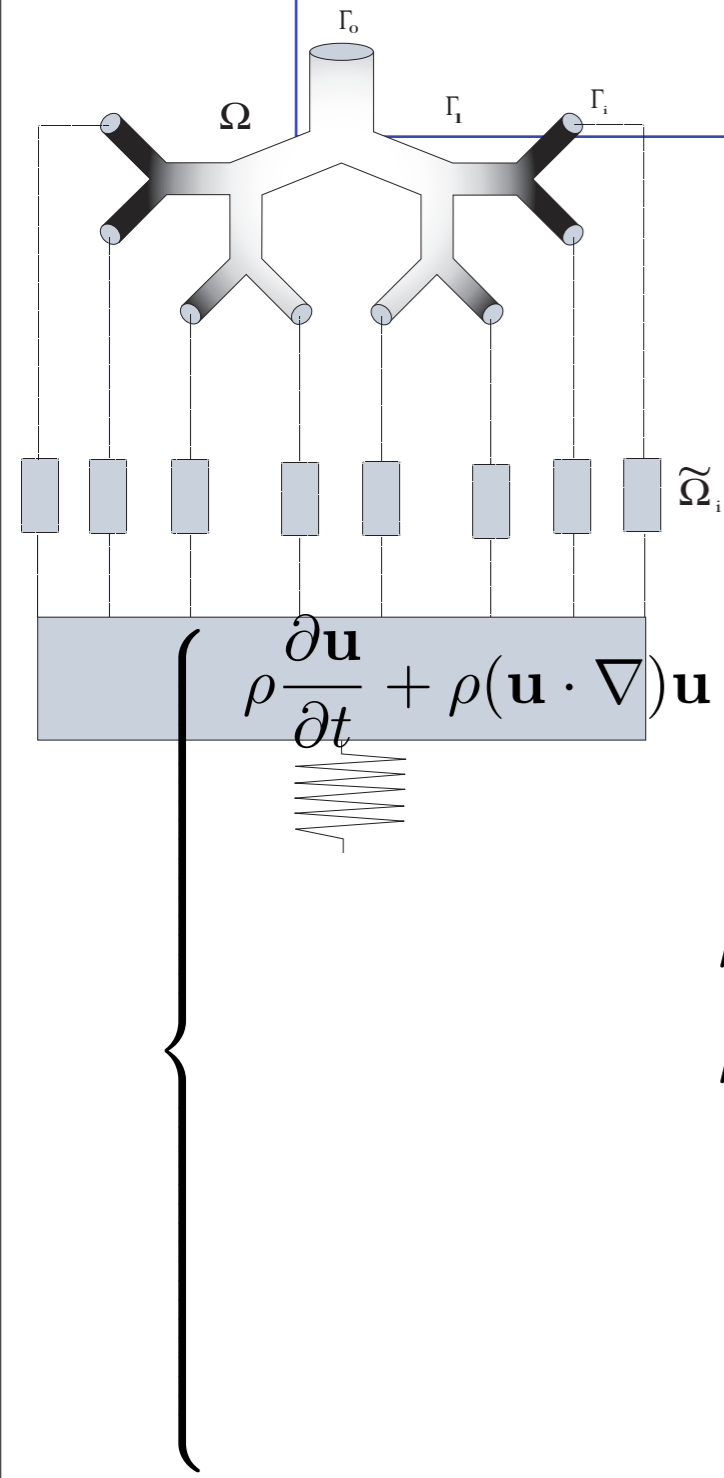
$$S\dot{x} = \sum_{i=1}^N \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} = - \int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n},$$

# Coupled System



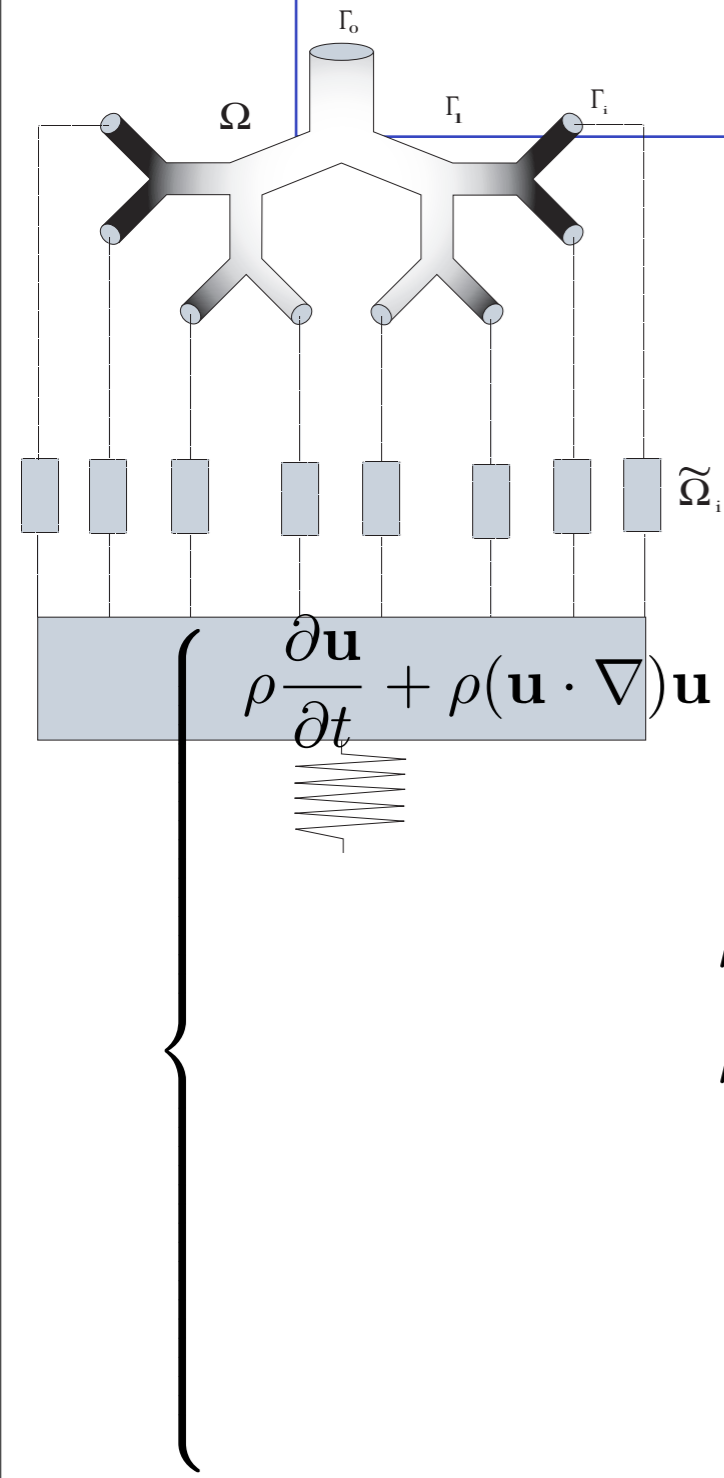
$$\left. \begin{aligned}
 \rho \frac{\partial \mathbf{u}}{\partial t} + \rho(\mathbf{u} \cdot \nabla) \mathbf{u} - \mu \Delta \mathbf{u} + \nabla p &= 0, & \text{in } (0, T) \times \Omega, \\
 \nabla \cdot \mathbf{u} &= 0, & \text{in } (0, T) \times \Omega, \\
 \mathbf{u} &= 0, & \text{on } (0, T) \times \Gamma_l, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_0 \mathbf{n} & \text{on } (0, T) \times \Gamma_0, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_a \mathbf{n} - R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \mathbf{n}, & \text{on } (0, T) \times \Gamma_i, \\
 & & i = 1, \dots, N, \\
 m \ddot{x} + kx &= f_{ext} + SP_a, \\
 S \dot{x} &= \sum_{i=1}^N \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} = - \int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n}.
 \end{aligned} \right\}$$

# Coupled System



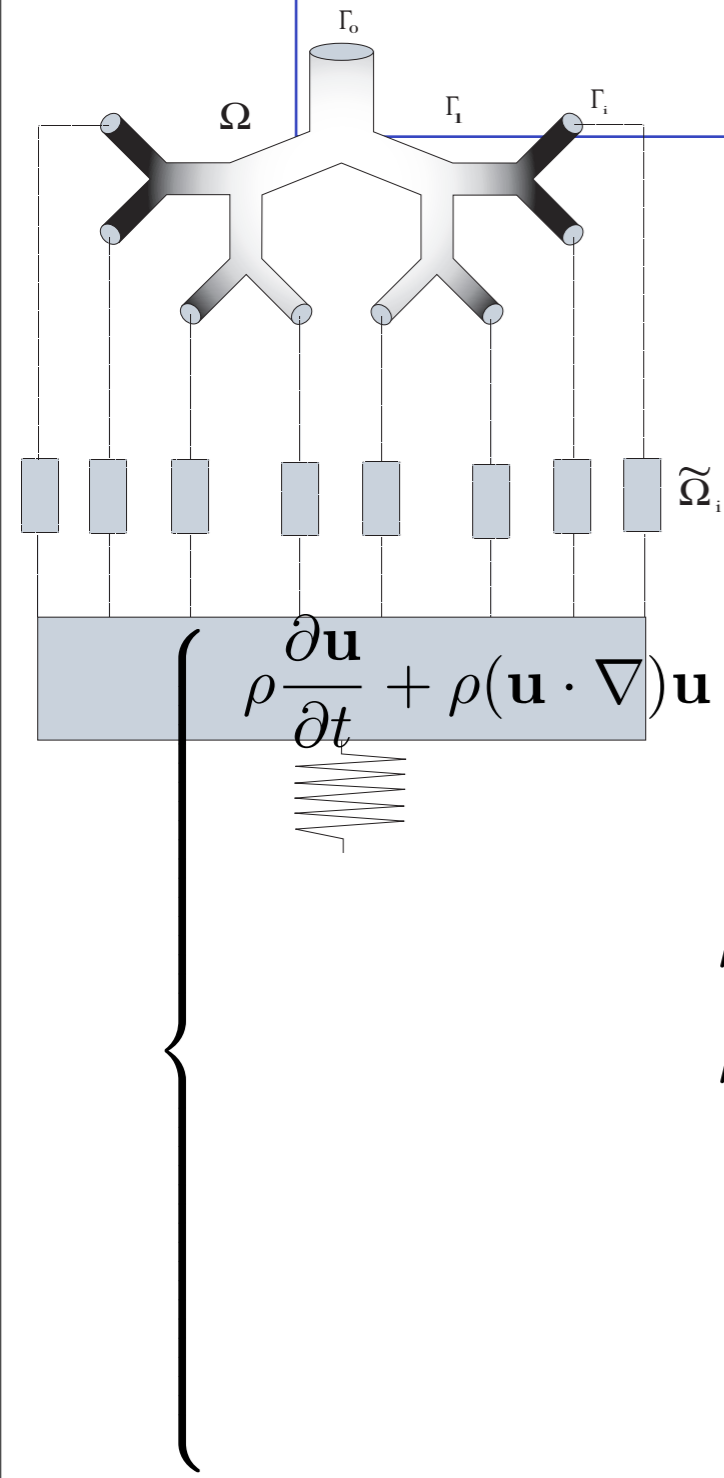
$$\left. \begin{aligned}
 \rho \frac{\partial \mathbf{u}}{\partial t} + \rho(\mathbf{u} \cdot \nabla) \mathbf{u} - \mu \Delta \mathbf{u} + \nabla p &= 0, & \text{in } (0, T) \times \Omega, \\
 \nabla \cdot \mathbf{u} &= 0, & \text{in } (0, T) \times \Omega, \\
 \mathbf{u} &= 0, & \text{on } (0, T) \times \Gamma_l, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_0 \mathbf{n} & \text{on } (0, T) \times \Gamma_0, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_a \mathbf{n} - R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \mathbf{n}, & \text{on } (0, T) \times \Gamma_i, \\
 & & i = 1, \dots, N, \\
 m \ddot{x} + kx &= f_{ext} + SP_a, \\
 S \dot{x} &= \sum_{i=1}^N \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} = - \int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n}.
 \end{aligned} \right\}$$

# Coupled System



$$\left. \begin{aligned}
 \rho \frac{\partial \mathbf{u}}{\partial t} + \rho(\mathbf{u} \cdot \nabla) \mathbf{u} - \mu \Delta \mathbf{u} + \nabla p &= 0, & \text{in } (0, T) \times \Omega, \\
 \nabla \cdot \mathbf{u} &= 0, & \text{in } (0, T) \times \Omega, \\
 \mathbf{u} &= 0, & \text{on } (0, T) \times \Gamma_l, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_0 \mathbf{n} & \text{on } (0, T) \times \Gamma_0, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_a \mathbf{n} - R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \mathbf{n}, & \text{on } (0, T) \times \Gamma_i, \\
 & & i = 1, \dots, N, \\
 m \ddot{x} + kx &= f_{ext} + SP_a, \\
 S \dot{x} &= \sum_{i=1}^N \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} = - \int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n}.
 \end{aligned} \right\}$$

# Coupled System



$$\left. \begin{aligned}
 \rho \frac{\partial \mathbf{u}}{\partial t} + \rho(\mathbf{u} \cdot \nabla) \mathbf{u} - \mu \Delta \mathbf{u} + \nabla p &= 0, & \text{in } (0, T) \times \Omega, \\
 \nabla \cdot \mathbf{u} &= 0, & \text{in } (0, T) \times \Omega, \\
 \mathbf{u} &= 0, & \text{on } (0, T) \times \Gamma_l, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_0 \mathbf{n} & \text{on } (0, T) \times \Gamma_0, \\
 \mu \nabla \mathbf{u} \cdot \mathbf{n} - p \mathbf{n} &= -P_a \mathbf{n} - R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \mathbf{n}, & \text{on } (0, T) \times \Gamma_i, \\
 & & i = 1, \dots, N, \\
 m \ddot{x} + kx &= f_{ext} + SP_a, \\
 S \dot{x} &= \sum_{i=1}^N \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} = - \int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n}.
 \end{aligned} \right\}$$

# Coupled System

By setting  $\bar{p} = p - P_a$ , by using the expression of the alveola pressure  $P_a = \frac{m}{S}\ddot{x} + \frac{k}{S}x - \frac{f_{ext}}{S}$  and the volume preserving equation  $S\dot{x} = -\int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n}$ , the coupled system can be written as follows:

$$\left\{ \begin{array}{ll} \rho \frac{\partial \mathbf{u}}{\partial t} + \rho(\mathbf{u} \cdot \nabla)\mathbf{u} - \mu \Delta \mathbf{u} + \nabla \bar{p} = 0, & \text{in } (0, T) \times \Omega, \\ \nabla \cdot \mathbf{u} = 0, & \text{in } (0, T) \times \Omega, \\ \mathbf{u} = 0, & \text{on } (0, T) \times \Gamma_l \\ \mu \nabla \mathbf{u} \cdot \mathbf{n} - \bar{p} \mathbf{n} = -P_0 \mathbf{n} - \frac{f_{ext}}{S} \mathbf{n} & \\ \quad - \frac{m}{S^2} \frac{d}{dt} \left( \int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n} \right) \mathbf{n} - \frac{k}{S^2} \left( \int_0^t \int_{\Gamma_0} \mathbf{u} \cdot \mathbf{n} - Sx_0 \right) \mathbf{n}, & \text{on } (0, T) \times \Gamma_0 \\ \mu \nabla \mathbf{u} \cdot \mathbf{n} - \bar{p} \mathbf{n} = -R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \mathbf{n}, & \text{on } (0, T) \times \Gamma_i \\ & i = 1, \dots, N \end{array} \right. \quad (1)$$

# Wellposedness

## Energy Balance

$$\begin{aligned}
 & \frac{d}{dt} \underbrace{\left( \frac{\rho}{2} \int_{\Omega} |\mathbf{u}|^2 + \frac{m}{2} |\dot{x}|^2 + \frac{k}{2} |x|^2 \right)}_{\text{Total energy}} + \underbrace{\mu \int_{\Omega} |\nabla \mathbf{u}|^2}_{\text{Dissipation within } \Omega} + \underbrace{\sum_{i=1}^N R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right)^2}_{\text{Dissipation in the subtrees}} \\
 = & - \underbrace{\frac{\rho}{2} \sum_{i=0}^N \int_{\Gamma_i} |\mathbf{u}|^2 (\mathbf{u} \cdot \mathbf{n})}_{\text{In/out-come of kinetic energy}} + \underbrace{P_0 S \dot{x}}_{\text{Power of inlet pressure}} + \underbrace{f_{ext} \dot{x}}_{\text{Power of ext. forces}} .
 \end{aligned}$$

# Wellposedness

- C. G., B. Maury, Y. Maday,  $p$  is replaced by the total pressure  $p + \rho|\mathbf{u}|^2/2$
- C. G., B. Maury, A. Soualah, with  $\mathbf{u} = \lambda_i \mathbf{U}_i$  on  $\Gamma_i$ , existence of weak solutions
  - locally in time for any data
  - for all time for small enough data
- L. Baffico, C. G., B. Maury, existence of “strong” solutions
  - locally in time for any data
  - for all time for small enough data
- **Related works:** [Heywood, Rannacher, Turek] [Quarteroni, Veneziani], [Vignon et al]...

$$V = \{\mathbf{v} \in H^1(\Omega)^d, \nabla \cdot \mathbf{v} = 0, \mathbf{v} = 0 \text{ on } \Gamma_\ell\}.$$

$$H = \overline{V}^{L^2},$$

We denote by  $(\cdot, \cdot)_0$  the scalar product on  $H \times H$  defined by

$$(\mathbf{v}, \mathbf{w})_0 = \rho \int_{\Omega} \mathbf{v} \cdot \mathbf{w} + \frac{m}{S^2} \left( \int_{\Gamma_0} \mathbf{v} \cdot \mathbf{n} \right) \left( \int_{\Gamma_0} \mathbf{w} \cdot \mathbf{n} \right),$$

and by  $\|\cdot\|_0$  the associated norm. Next we set

$$a_1(\mathbf{v}, \mathbf{w}) = \mu \int_{\Omega} \nabla \mathbf{v} : \nabla \mathbf{w} + \sum_{i=1}^N R_i \left( \int_{\Gamma_i} \mathbf{v} \cdot \mathbf{n} \right) \left( \int_{\Gamma_i} \mathbf{w} \cdot \mathbf{n} \right),$$

Finally we introduce an operator  $A$  whose **eigenvectors will constitute the Galerkin basis** used to build our sequence of approximated solutions.

The operator  $A$  is defined on  $H$  as follows:

$$D(A) = \{\mathbf{v} \in V, |a_1(\mathbf{v}, \mathbf{w})| \leq C\|\mathbf{v}\|_0, \forall \mathbf{w} \in V\},$$

$$(A\mathbf{v}, \mathbf{w})_0 = a_1(\mathbf{v}, \mathbf{w}), \forall (\mathbf{v}, \mathbf{w}) \in D(A) \times V.$$

# Numerical methods

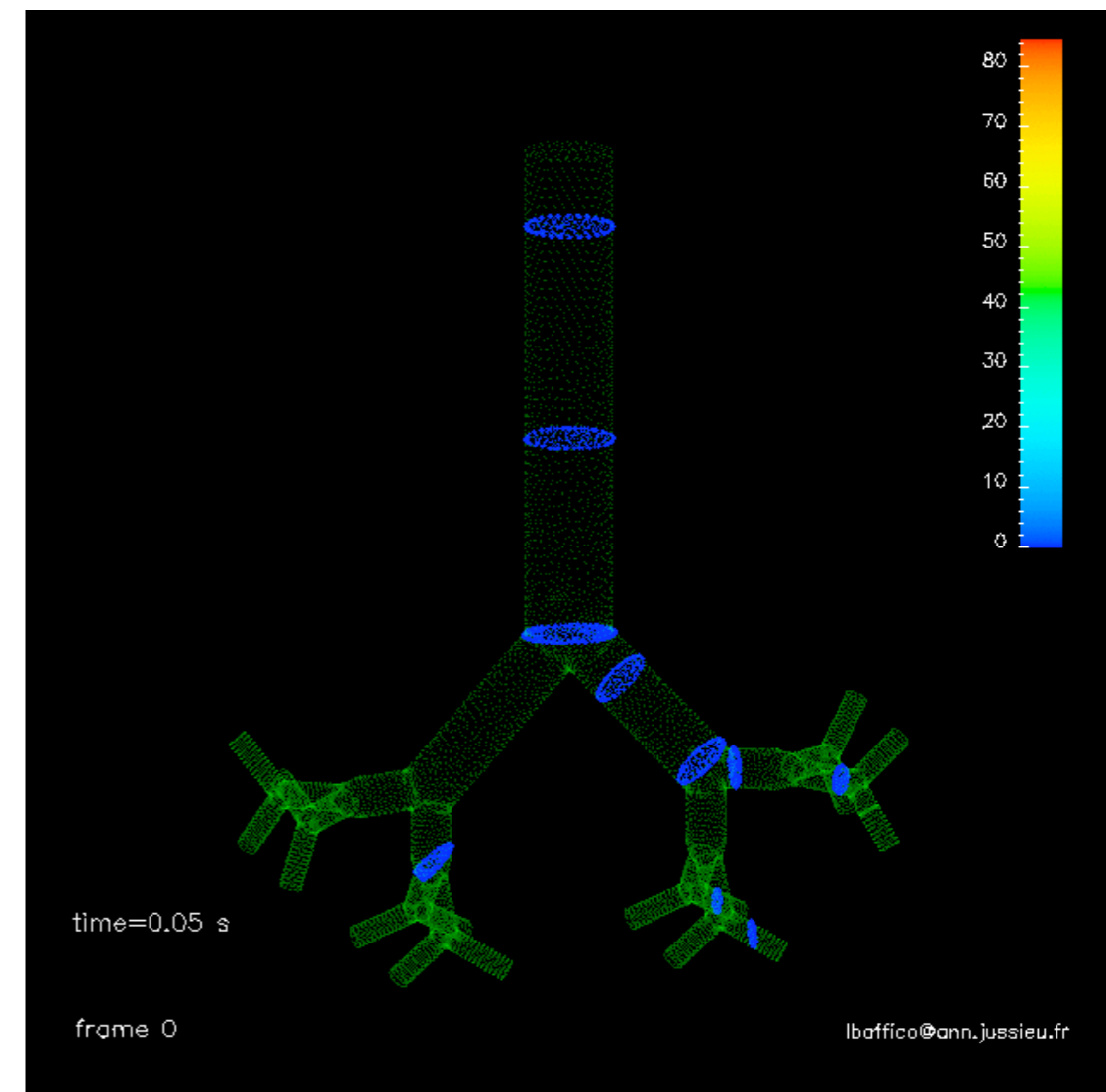
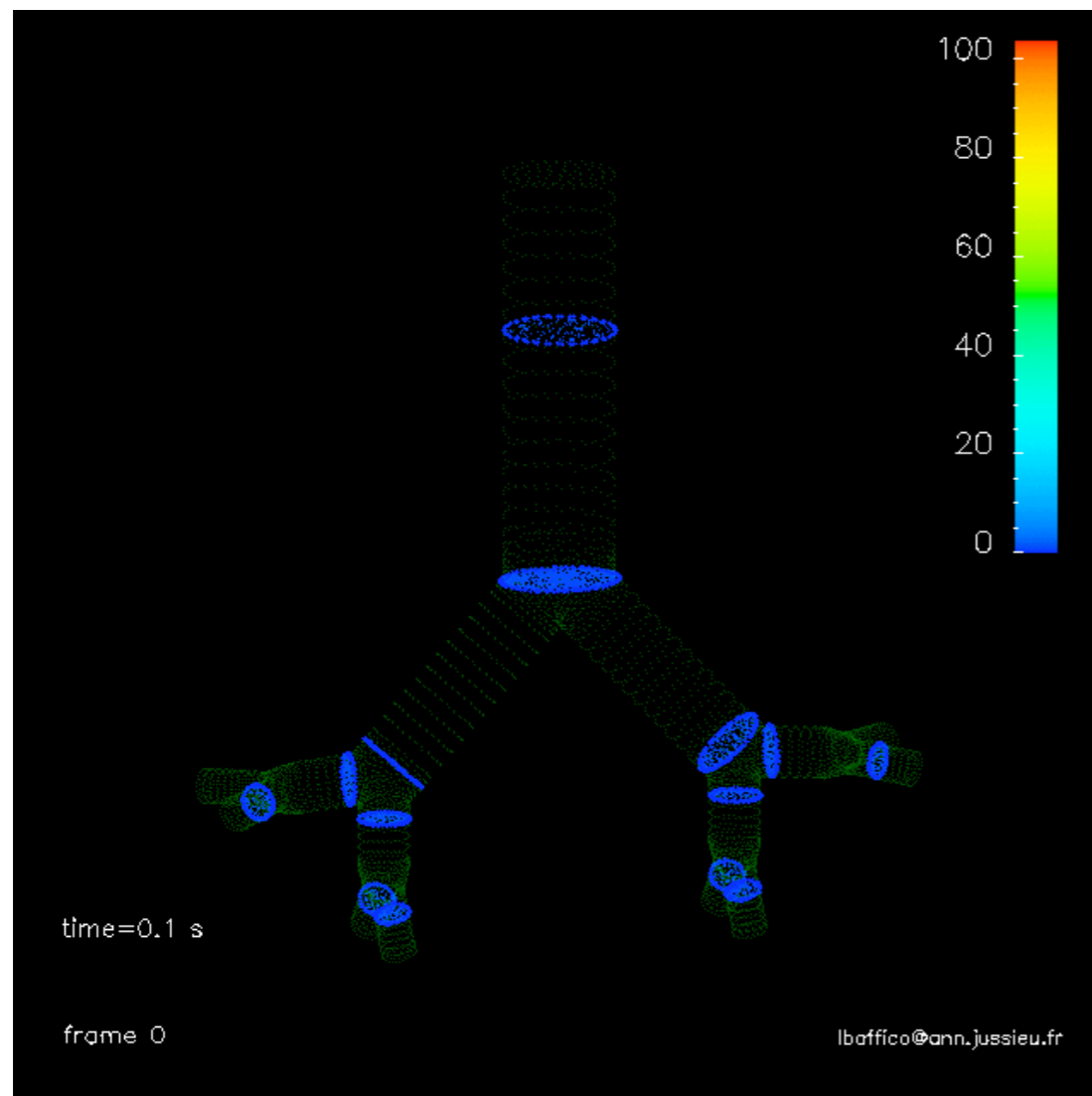
## Discretization

$$\begin{aligned}a(\mathbf{u}^{n+1}, \mathbf{v}) + b(\mathbf{v}, p^{n+1}) &= l^{n+1}(\mathbf{v}) \\ b(\mathbf{u}^{n+1}, q) &= 0 \quad \forall q \in L^2(\Omega), \\ x^{n+1} &= x^n - \frac{\delta t}{S} \int_{\Gamma_0} \mathbf{u}^{n+1} \cdot \mathbf{n}\end{aligned}$$

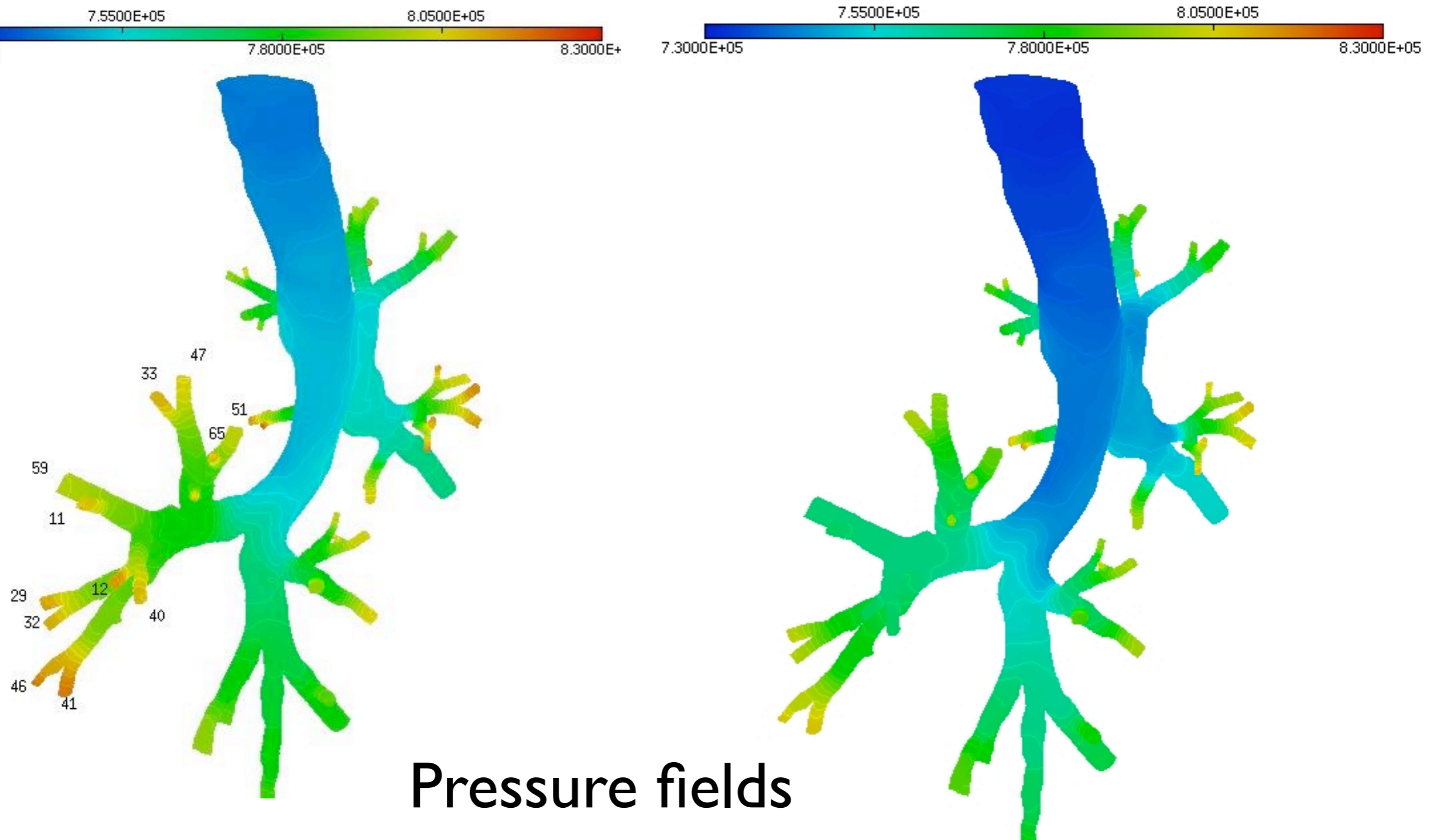
where

$$\begin{aligned}a(\mathbf{u}, \mathbf{v}) &= \frac{\rho}{\delta t} \int_{\Omega} \mathbf{u} \cdot \mathbf{v} + 2\mu \int_{\Omega} \nabla \mathbf{u} : \nabla \mathbf{v} \\ &+ \sum_{i=1}^N R_i \left( \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \left( \int_{\Gamma_i} \mathbf{v} \cdot \mathbf{n} \right) \\ &+ \frac{1}{S^2} \left( \frac{m}{\delta t} + k\delta t \right) \left( \sum_{i=1}^N \int_{\Gamma_i} \mathbf{u} \cdot \mathbf{n} \right) \left( \sum_{i=1}^N \int_{\Gamma_i} \mathbf{v} \cdot \mathbf{n} \right),\end{aligned}$$

# Numerical simulations

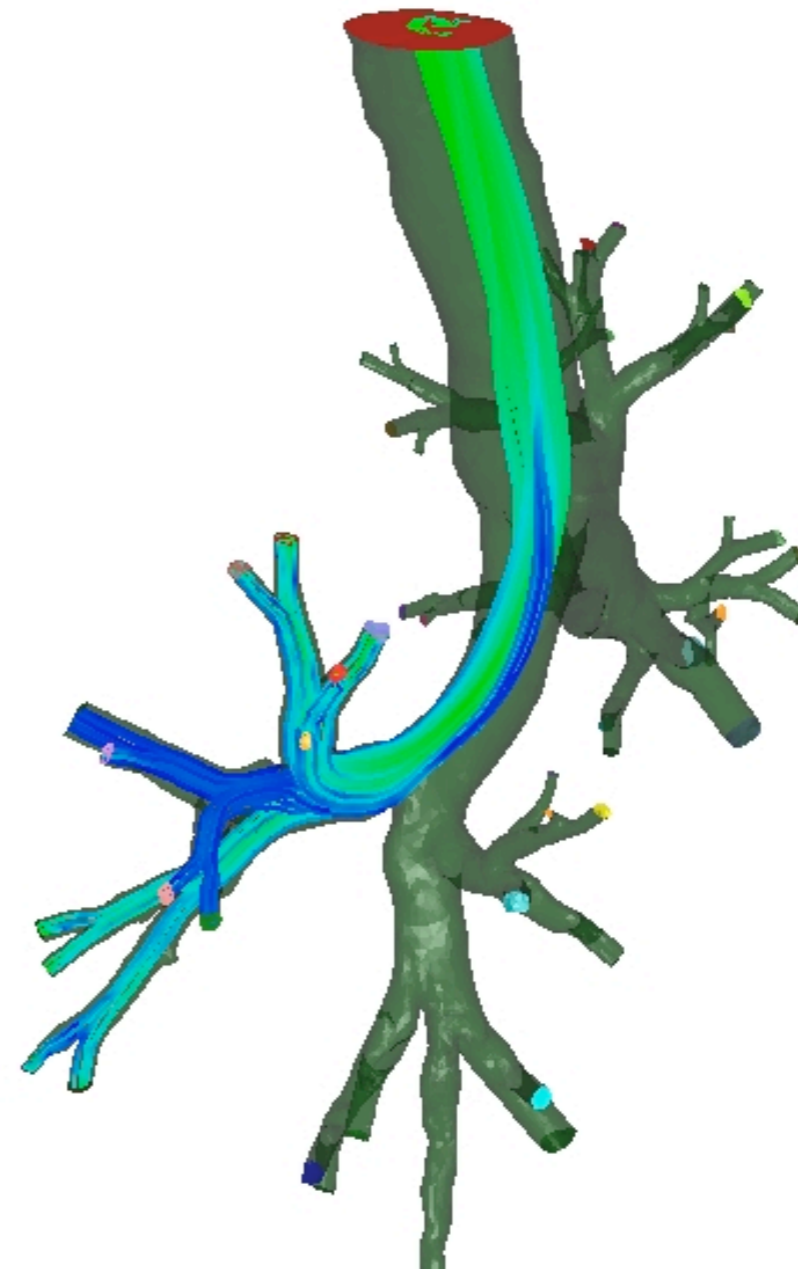
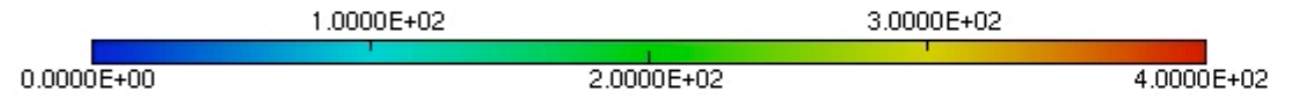
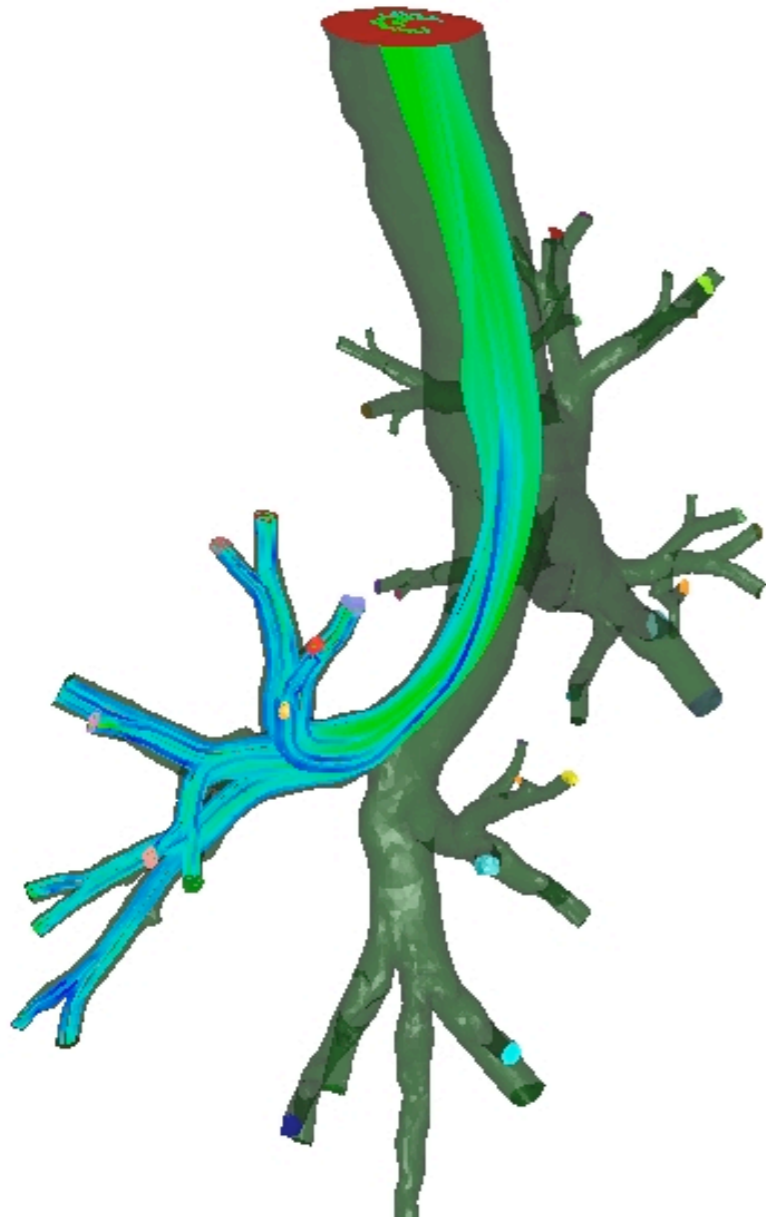
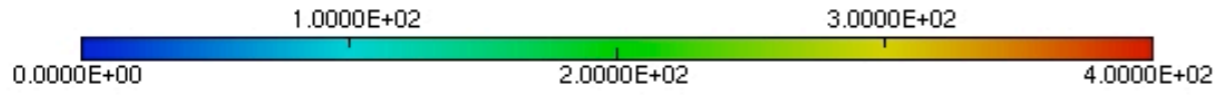


# Numerical simulations



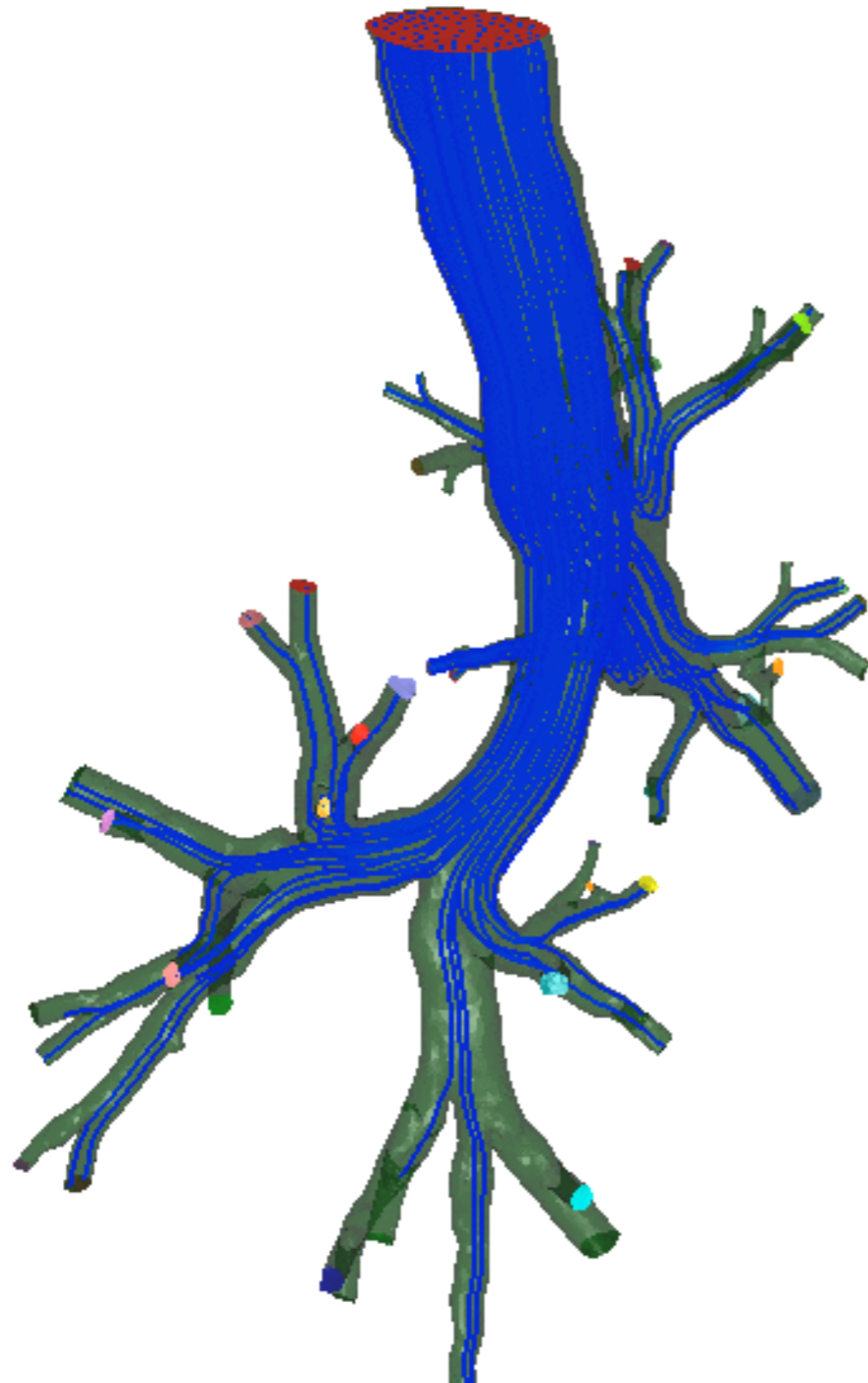
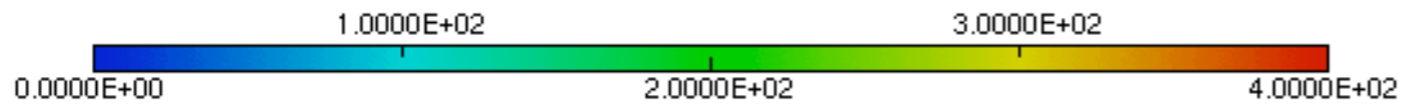
Same geometry as in [C. Fetita, S. Mancini, D. Perchet, F. Preteux, M. Thiriet, L. Vial]

# Numerical Simulations

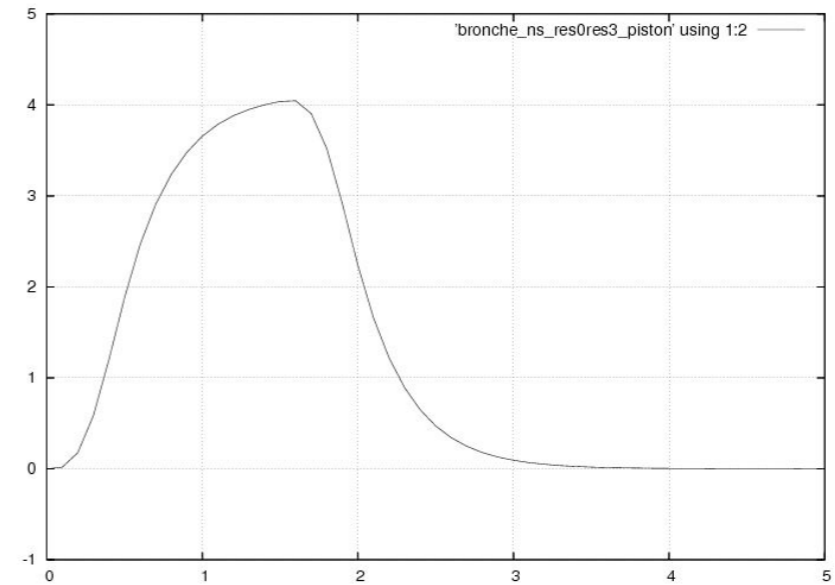


Streamlines

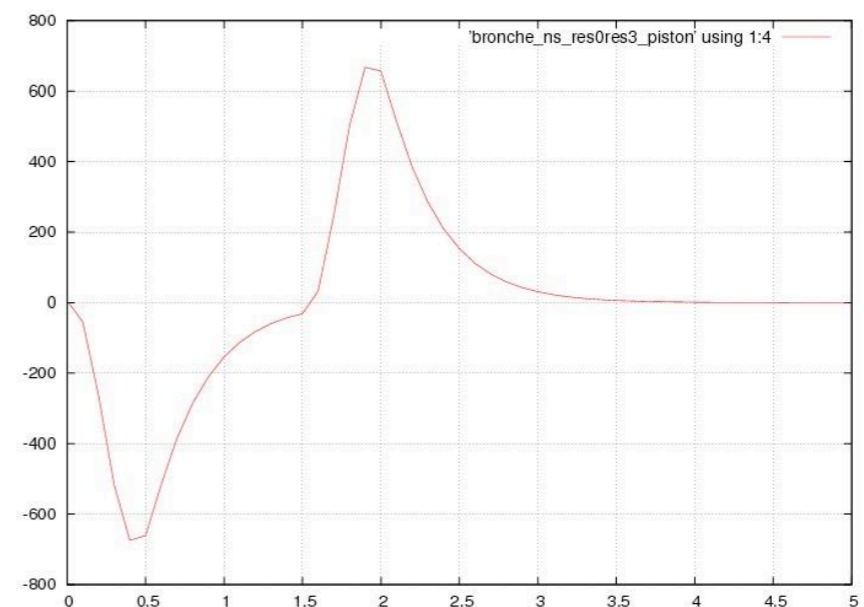
# Numerical simulations



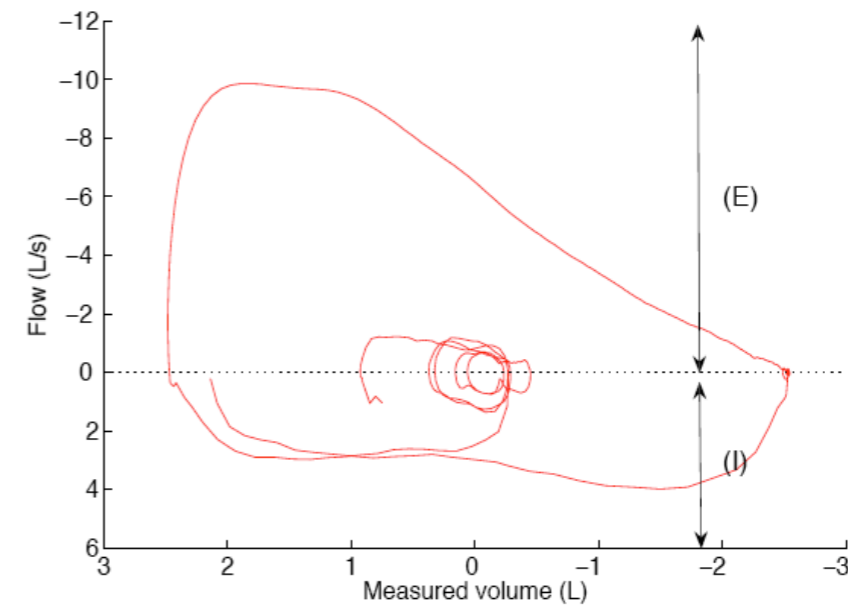
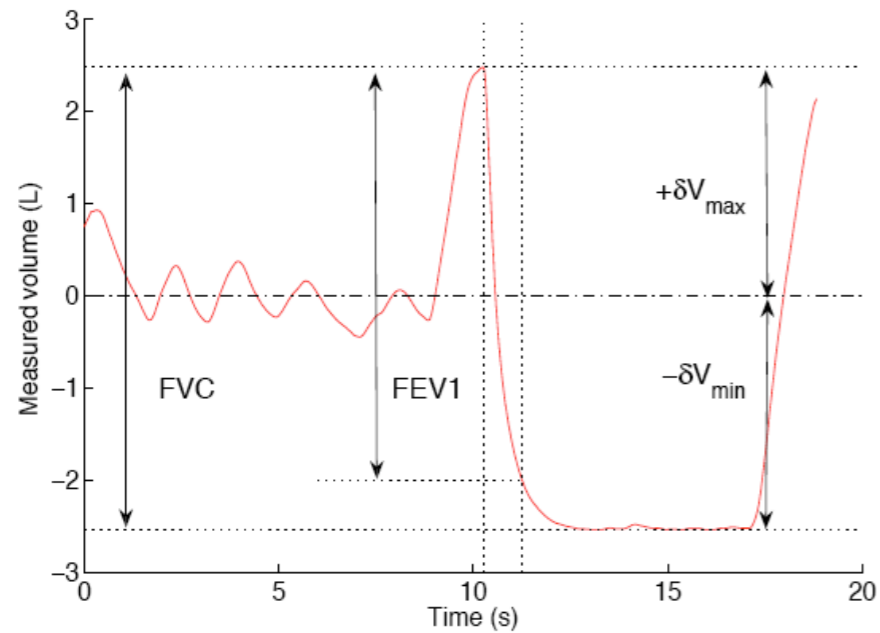
## Displacement



## Flux



# Improvements



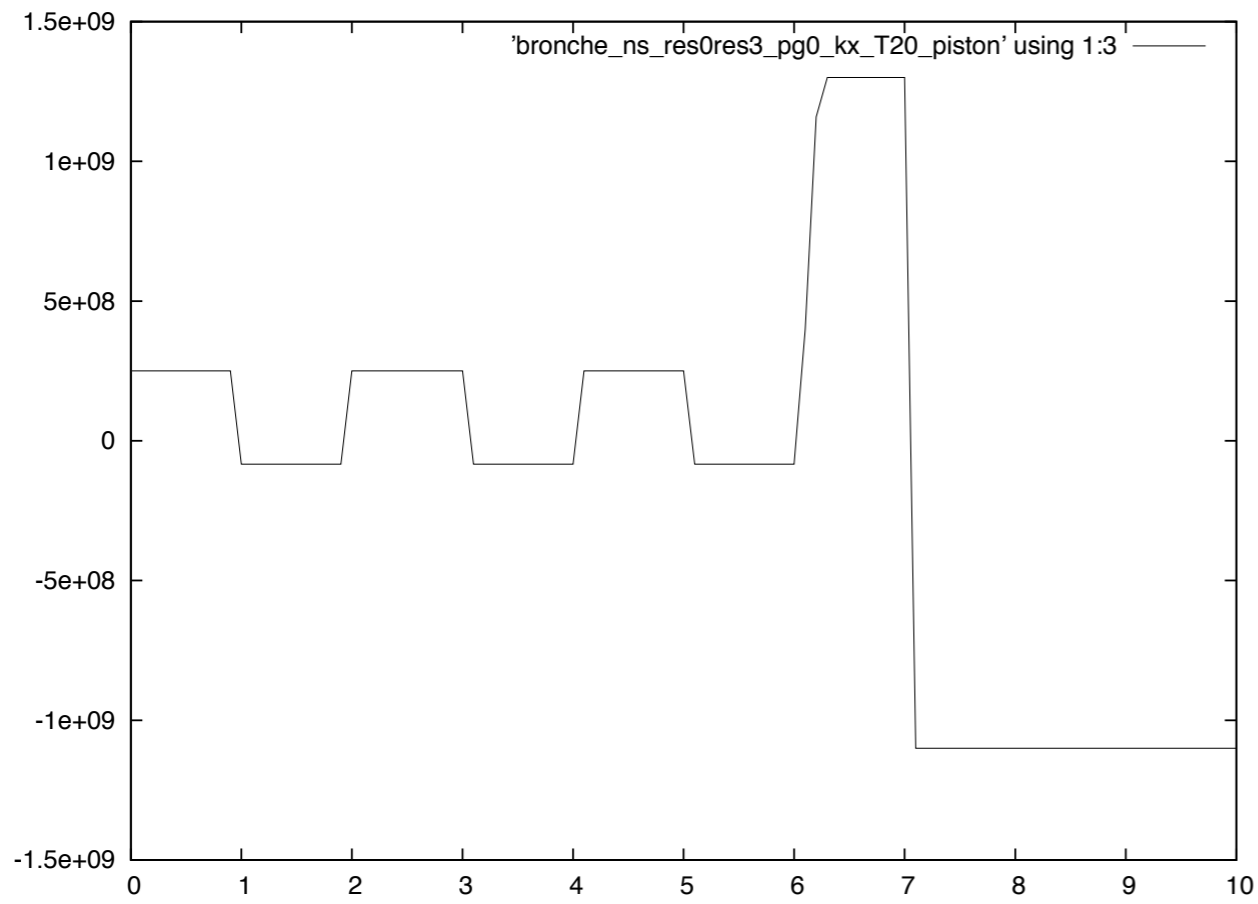
Following the work of [S. Martin](#), [M. Maury](#), [T. Similovski](#), [C. Strauss](#) and in order to take into account the limitation of the lung volume we can consider a nonlinear spring constant

$$k(x) = k_0 + k^{(e)}(x) + k^{(i)}(x),$$

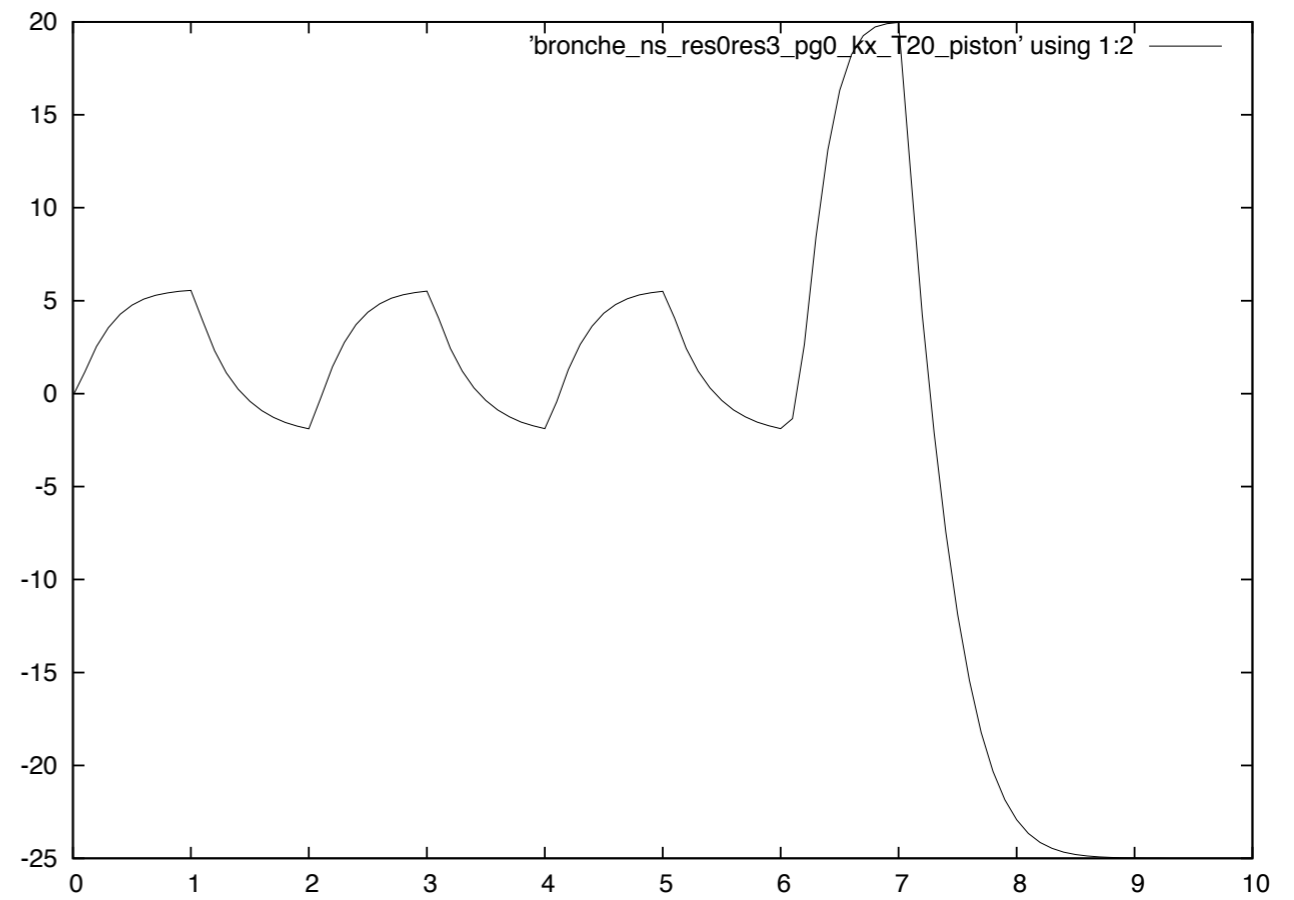
with

$$k^{(e)}(x) = \begin{cases} (f_{min}/x_{min} - k_0)x/x_{min}, & \text{if } x < 0 \\ 0, & \text{if } x \geq 0, \end{cases}$$

$$k^{(i)}(x) = \begin{cases} 0, & \text{if } x < 0 \\ (f_{max}/x_{max} - k_0)x/x_{max}, & \text{if } x \geq 0 \end{cases}$$



External force



Air volume

# Air - spray coupling

Ph.D. thesis of A. Moussa (supervised by L. Desvillettes and M. Filoche)

- Fluid Flow: Navier-Stokes equations
- Aerosol: Kinetic approach - Deposition on the bronchial wall, no secondary droplets

# Air - Spray Coupling

- Spray: probability density function  $f(t, x, v, r, \dots)$  solving a kinetic equation (Vlasov, Boltzmann...)
- Fluid: density  $\rho(t, x)$ , velocity  $u(t, x)$ , pressure  $p(t, x)$ , ... solving Navier-Stokes system

$$\left\{ \begin{array}{l} \partial_t(\alpha \rho) + \nabla_x \cdot (\alpha \rho u) = 0 \\ \partial_t(\alpha \rho u) + \nabla_x \cdot (\alpha \rho u \otimes u) - \Delta_x u + \nabla_x p = \mathcal{F}_{\text{spray}} \\ \partial_t f + \nabla_x \cdot (f v) + \nabla_v \cdot (f a) + \partial_r(f \Phi) = Q(f, f) \end{array} \right.$$

# Classification

- $Q(f, f)(t, x, v, r)$  droplets interaction operator
- $\alpha(t, x) = 1 - \int_{v, r} \frac{m(r)}{\rho_{\text{drop}}} f(t, x, v, r) dv dr$   
fluid volume fraction (must remain near 1)
- $\mathcal{F}_{\text{spray}}(t, x) = - \int_{v, r} m(r) a(t, x, v, r) f(t, x, v, r) dv dr$   
force of the spray on the fluid

| spray                               | $Q(f, f)$ | $\alpha$ | $\mathcal{F}_{\text{spray}}$ |
|-------------------------------------|-----------|----------|------------------------------|
| very thin                           | 0         | 1        | 0                            |
| thin                                | 0         | 1        | $\mathcal{F}_{\text{spray}}$ |
| mod. thick                          | 0         | $\alpha$ | $\mathcal{F}_{\text{spray}}$ |
| thick                               | $Q(f, f)$ | $\alpha$ | $\mathcal{F}_{\text{spray}}$ |
| two fluids with a mixture behaviour |           |          |                              |

# Are respiratory aerosols very thin or only thin sprays?

- Experimental studies give various answers!
- they are **very thin** sprays [Grotberg...].
- they are **thin** sprays [Chigier, Corcoran...].

# Numerical Method

## Numerical particle method

$$f(t, x, v) = \sum_{p=1}^N \omega_p(t) \delta_{x_p(t)}(x) \delta_{v_p(t)}(v)$$

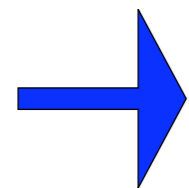
- $N$  total number of numerical particles,
- $t \mapsto (x_p(t), v_p(t))$  trajectory of the numerical  $p$  in the phase space,
- $\omega_p(t)$  representativity of particle  $p$ .

Coupling

Staggered scheme

# Futur Work

- Use this model to obtain physiological results in the proximal part (by modifying the resistance and the spring stiffness)
- Couple it with aerosol transport



Comparison with experimental results  
(INSERM Tours)